

IXO mission concept

- 1 – Introduction**
- 2 – IXO mission requirements
- 3 – IXO mission analysis
- 4 – IXO configuration
- 5 – IXO instrument module
- 6 – IXO service module
- 7 – IXO mirror assembly
- 8 – Options
- 9 – Conclusion

IXO mission terms of reference

-Input elements to IXO configuration include:

- 1- A single large X-ray mirror assembly compatible with both pore optics and slumped glass technology
- 2 - An extensible optical bench to reach $F=20$ to 25m + ways to maximise A_{eff} above 6 keV
- 3 - Instrument include a wide field imager, a high resolution non-dispersive spectrometer, an X-ray grating spectrometer + instruments with modest resources
- 4 - The IXO concept must be compatible with both Ariane V and Atlas V 551 launchers.

IXO CDF objectives

1 - Mirror assembly accommodation concept:

- pore optics technology and compatibility with slumped glass technology

2 - Design service module:

- Ariane V and compatibility with ATLAS V launcher

3 - Design instrument support platform:

- WFI+HXI, CSI, XGS (CAT), HTRS, XPOL

4 - Programmatic, organisation and possible ESA contributions (< 650 MEuros):

two main scenarios:

ESA delivers the IXO mirror assembly

NASA delivers the IXO mirror assembly

5 - Options

Focal length extension (> 20 m)

Retractable transmission grating concept

(+ estimate X-ray events time stamping accuracy)

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IXO mission requirements: scientific performance

Mirror Effective Area	3 m² @ 1.25 keV ~1 m² @ 6 keV ~350 cm² @ 30 keV	Black hole evolution, large scale structure, cosmic feedback, EOS Strong gravity, EOS Cosmic acceleration, strong gravity
Spectral Resolution	2.5 eV from 0.3 - 7.0 keV E/ Δ E > 1250 from 0.3–1 keV with area > 1,000 cm ² for point sources	Black Hole evolution, Large scale structure Missing baryons using tens of background AGN
Angular Resolution	≤ 5 arc sec HPD (0.3 – 10 keV) ≤ 15 arc sec HPD (10 - 40 keV)	Large scale structure, cosmic feedback, black hole evolution, missing baryons Black hole evolution
Field of View	2 x 2 arc min with ΔE < 2.5 eV 5 x 5 arc min with Δ E < 10 eV > 14 x 14 arc min with ΔE < 150 eV (18 arcmin at 20 m focal length)	Galaxy Clusters, cosmic feedback Galaxy Clusters Black hole evolution, galaxy clusters
Count Rate	1 Crab with < 10% deadtime Δ E < 200 eV	Strong gravity, EOS

IXO mission requirements: launcher and orbit

- Launcher: Ariane-5 ECA & Atlas 5
 - Launcher performance Ariane 5 (excl. adapter) ≈ 6170 Kg
 - Launcher performance Atlas 5 (excl. adapter) ≈ 6108 Kg
- Target Orbit: direct launch into L2 (similar ΔV budget for both launchers)
- 5 Year Mission (with consumables sized for a 10 years mission)
- Launch ≈ 2020

Preliminary IXO pointing and optical bench stability requirements

Preliminary image quality error budget (HEW on-axis at 1 keV):

- Mirror module manufacturing errors:	4.30 arcsec
- Optical design (conical approx.~ 3 arcsec)	
- Mirror figuring errors:	
- Mirror mid-frequencies errors & surface roughness:	
- Mirror plate alignment/confocality:	
- Mirror assembly system errors:	1.20 arcsec
- Assembly and integration	
- 1 g release	
- Thermal environment	
- Other (e.g. moisture release)	
- S/C pointing and optical bench distortions:	2.00 arcsec
- Events relative lateral measurement accuracy	
- Absolute longitudinal displacement errors	
- Margin: (including PSF sampling/detector pixel size)	1.00 arcsec
<hr/>	
Total (assuming RSS summation):	5.00 arcsec

Preliminary IXO pointing and optical bench stability requirements

Low f MA pointing requirements (MA ref. frame vs absolute ref. frame):

- Mirror assembly Absolute Pointing Error < 5 arcsec
- Mirror assembly Absolute Pointing Measurement Accuracy < 0.7 arcsec (on ground reconstruction)

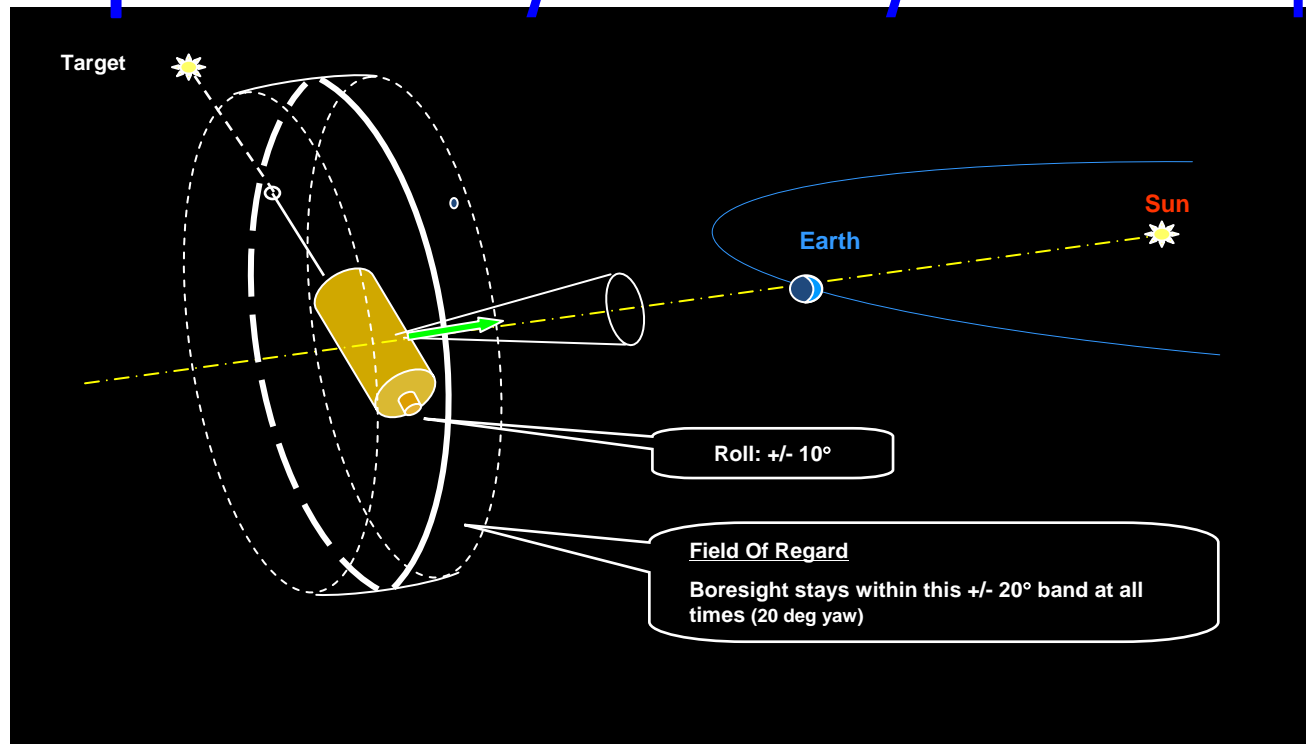
Low f detector positioning errors (detector ref. frame vs MA ref. frame):

- Detector absolute position measurement error (including uncalibrated OB static and low f distortion) < 0.07 mm
- Detector defocussing < 0.65 mm
- Static and low f optical bench distortions + detector lateral positioning errors < 0.5 mm (maximum amplitude without pointing correction or calibration accuracy with pointing correction)

High f MA pointing error + high f OB distortions < 110 μm (or 1.1 arcsec)

Torsional requirements: < 0.05 degree (XGS)

IXO mission requirements: sky accessibility and slew requirements



Field of Regard	<ul style="list-style-type: none"> Pitch: $\pm 20^\circ$ off Sunline Yaw: $\pm 180^\circ$ Roll: $\pm 10^\circ$ (with a goal of 20°) off Sunline
Slew	<ul style="list-style-type: none"> Target Of Opportunity observed in less than 24h

IXO mission requirements: observation scenario

Number of Targets:

- 210 targets in 1 year.
- 77 observations were made of the same target with >3 instruments
- 34 targets required repeated (typically 4) observations spread over time.
- 7 targets needed mosaicing of between 2×2 and 10×10 pointings to cover 1 sq degree.

Exposure Times

- Minimum Exposure: 10 ks
- Maximum Exposure: 1000 ks
- Mean Exposure: 70.4 ks

Instrument Utilisation

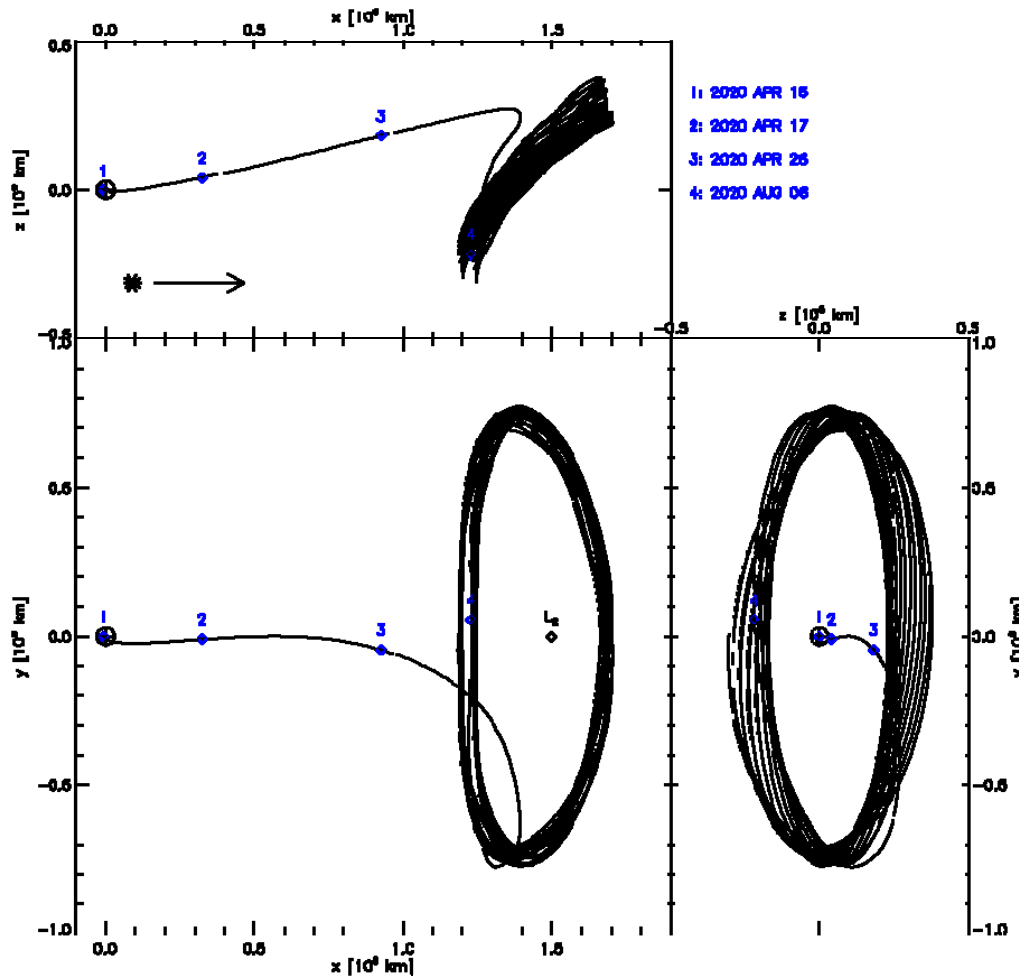
- XGS: assumed to be always operating.
- WFI: 48%
- NFI: 31%
- HTRS: 14%
- XPOL: 5%
- HXC: 1 % (as prime, assumed to be behind WFI)

→183 instrument exchange/year

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IXO reference trajectory and Δv Budget



manoeuvre	Δv [ms ⁻¹]
perigee velocity correction	28.0
launcher dispersion correction	34.0
transfer	3.0
orbit insertion	0.0
station keeping (10y)	20.0
de-orbit	0.0
wheel off-loading correction	7.7
total	85.0
margin (5%)	4.63
thruster mounting $1/\cos(28^\circ)$	11.7
total Δv budget	109.4

L2 particle (protons) environment

- LRAD – now L2CPE: NASA developed statistical model of plasma densities and temperatures in L2 (Solar wind, Plasma sheet, Magnetosheath, Lobe and Mantle)

- Blackwell et al [2000], using LRAD, looked at the effect of L2 halo orbit amplitude on the flux statistics for electrons and protons.

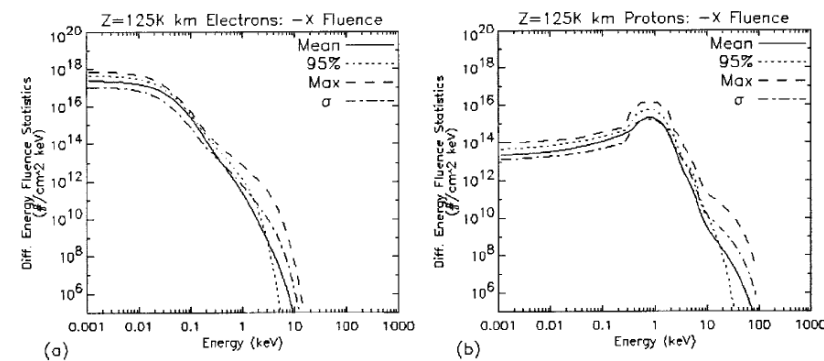


Figure 10. Fluence Statistics for a Single 125,000 km Z-Amplitude Halo Orbit. Solar wind values from 1992 were used to drive the magnetosheath and magnetotail variations for the 6 month orbital period. Fluence is dominated by the bulk flow contribution near 1 keV for the ions.

→ No change in flux of protons from 10keV to 100keV depending on halo orbit amplitude,

→ a consideration of Larmor radius for higher energy particles suggests that there should be no dependence on orbit amplitude for the higher energy protons too.

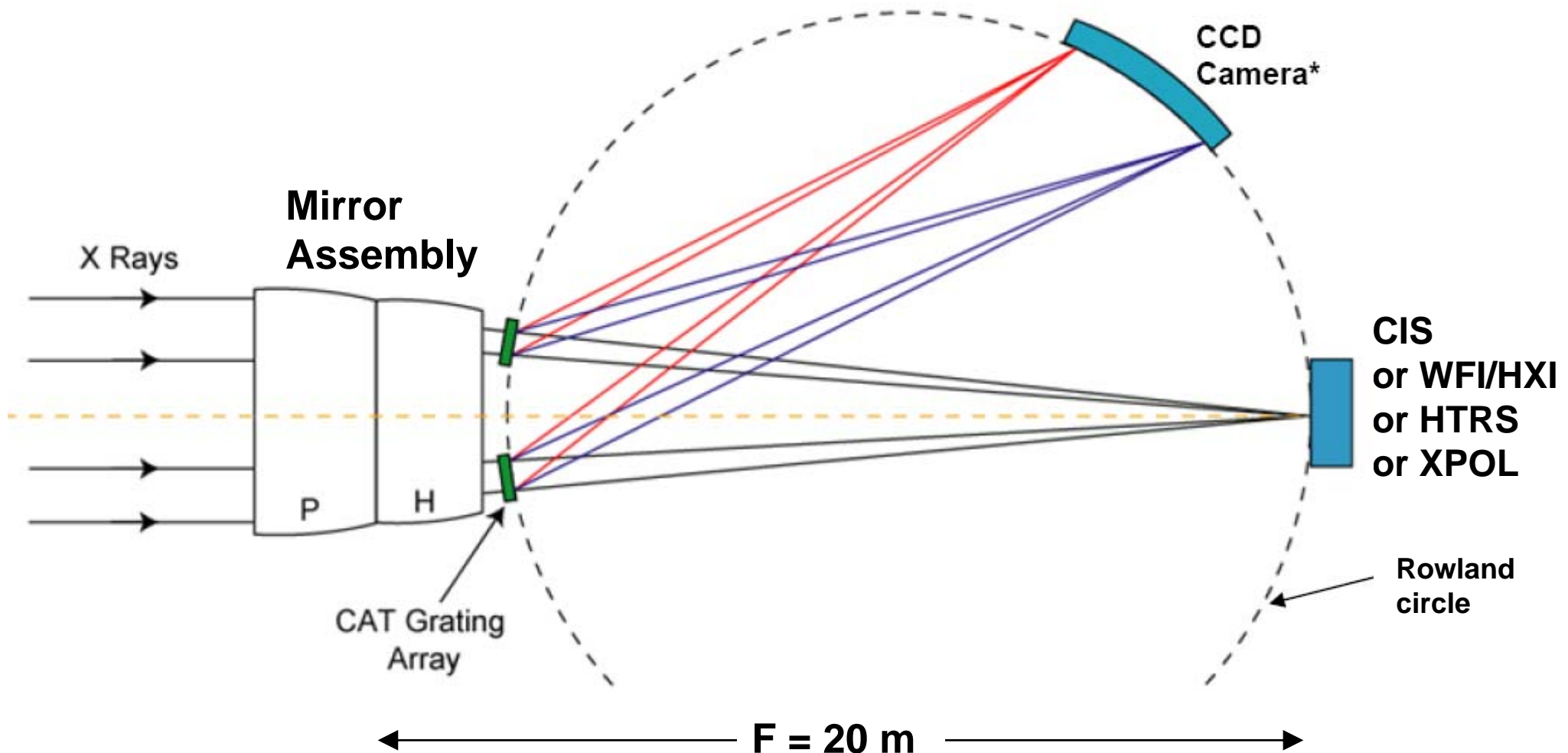
Table 1. 125,000 km Z-Amplitude Halo Orbit Satellite Location Summary

Number of Monte Carlo Runs =	1000	Total problem duration=	180.00000 days
Fraction of halo orbit spent inside individual regions:			
Solar Wind Region :	12.77 % (22.99 days)	N/S Lobe Region :	0.00 % (0.00 days)
Plasma Sheet Region :	3.22 % (5.80 days)	Plasma Mantle Region :	5.91 % (10.63 days)
Magnetosheath Region :	78.11 % (140.60 days)		

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IXO configuration



IXO configuration

X-ray telescope with high energy response

- large telescope focal length
- **deployable optical bench**

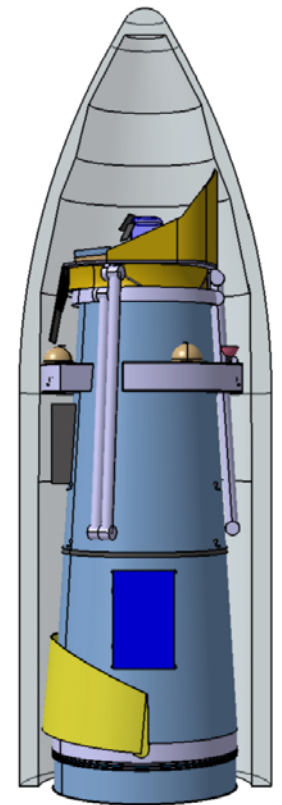
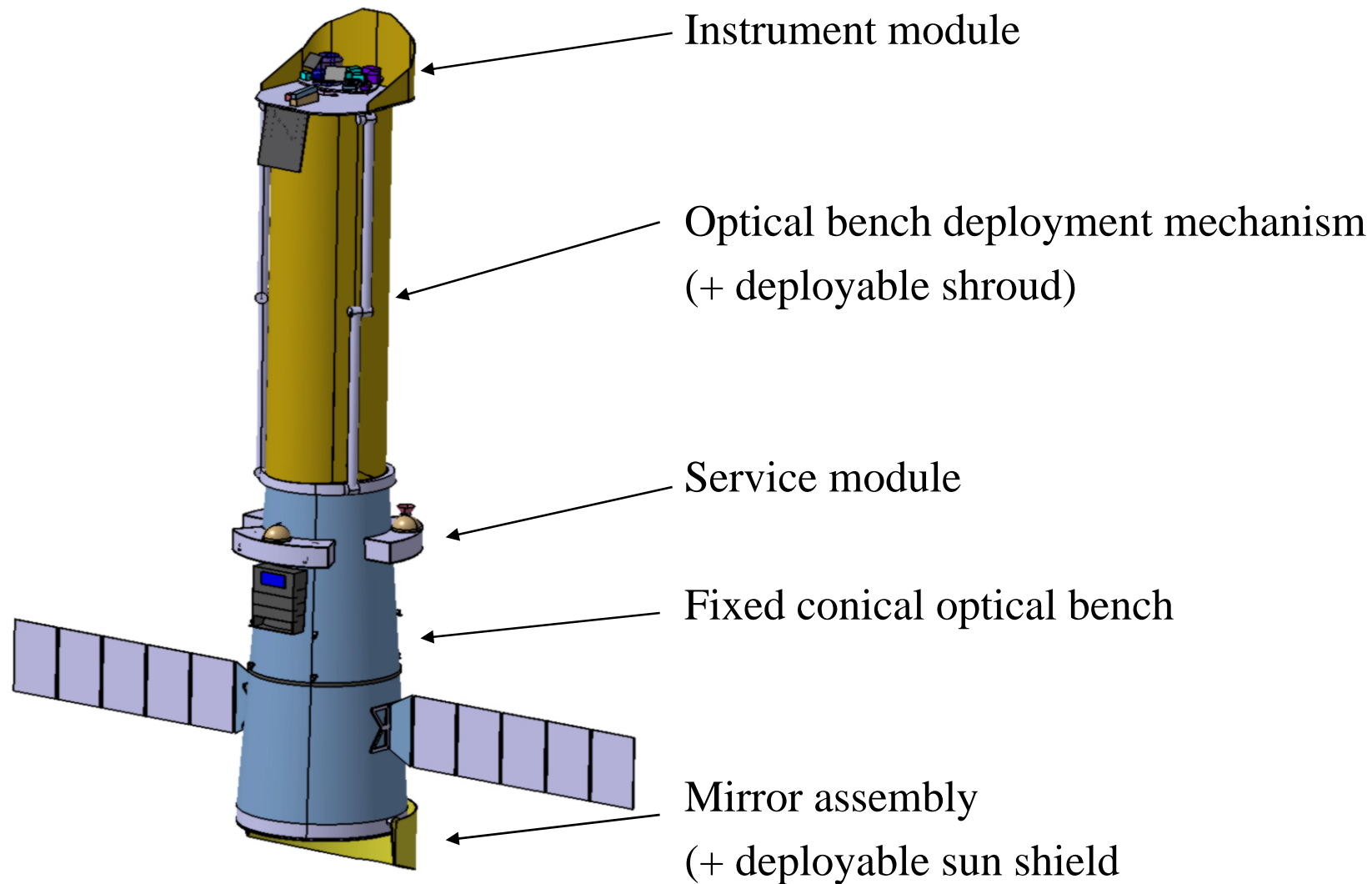
During science operation,

- the grating spectrometer is always operating
- any of the other 4 instruments can be placed at the focus of the X-ray telescope.
- **instrument exchange mechanism**

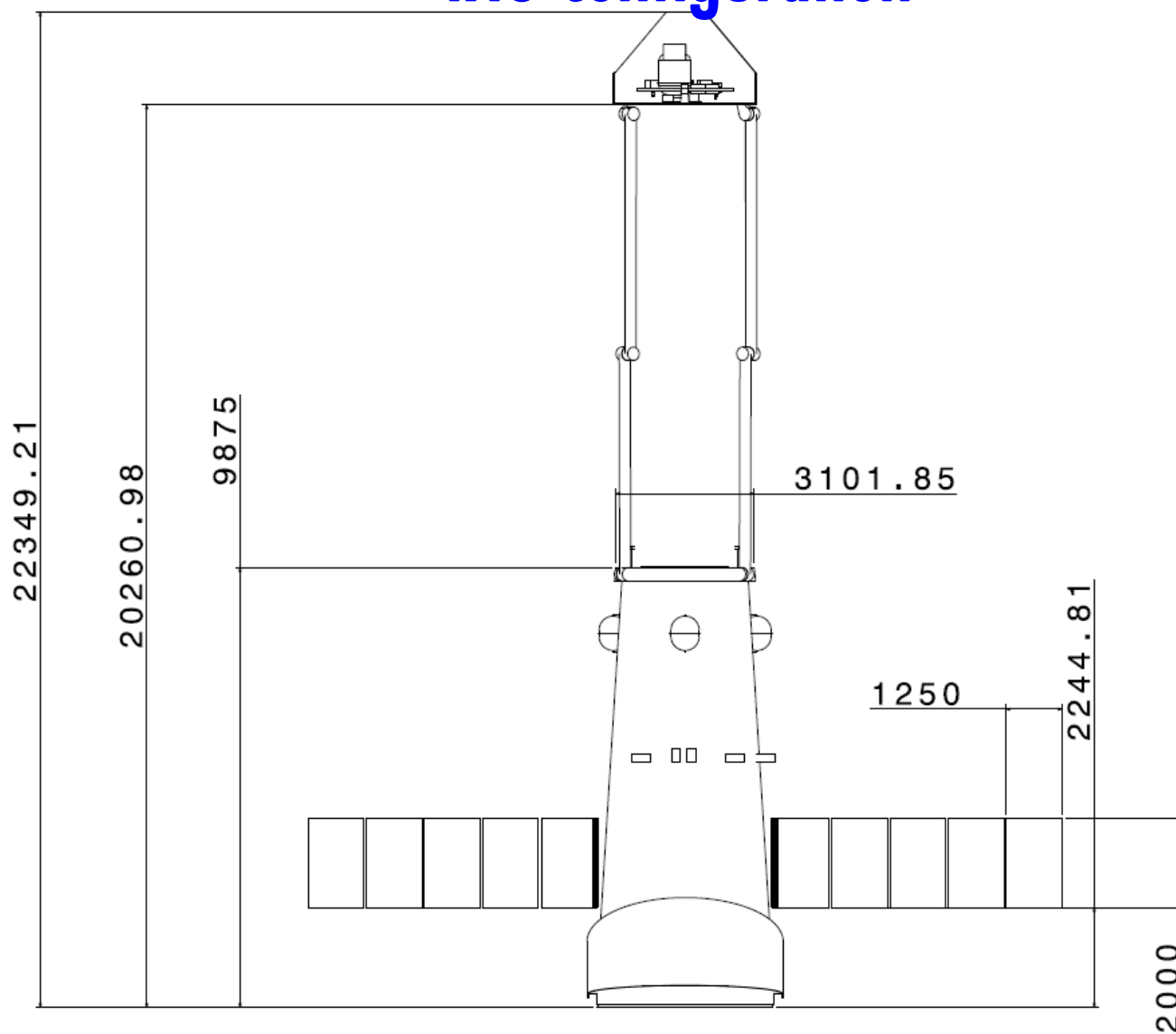
The instruments shall be protected from particle background and stray-light

- **cylindrical baffles and/or (deployable) shroud**

IXO configuration



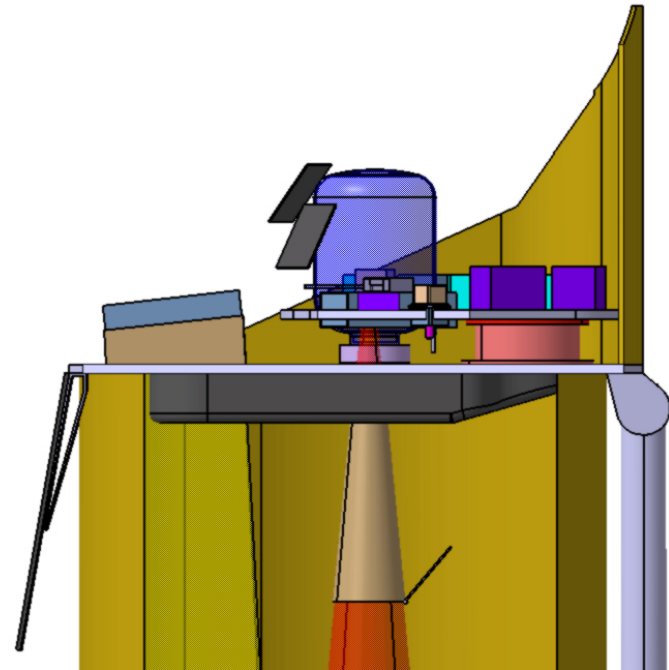
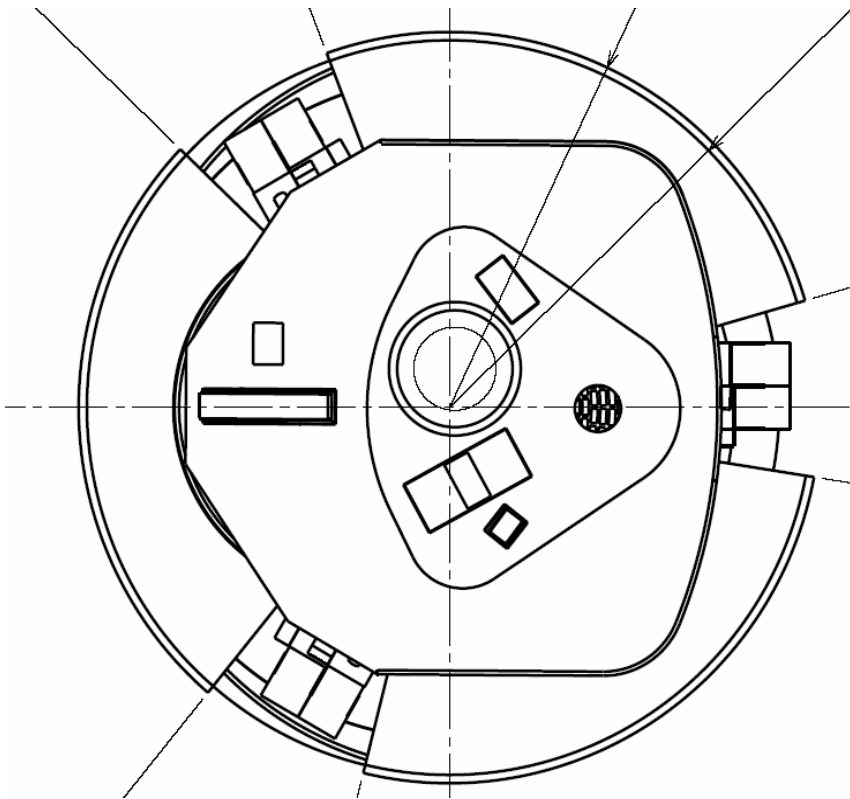
IXO configuration



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IXO instrument module: configuration



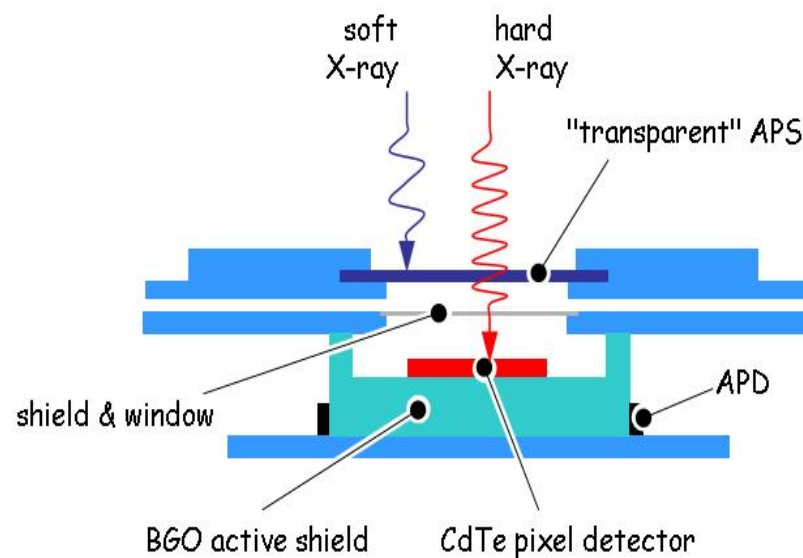
IXO instrument module: WFI+HXI

WFI specifications:

- Imaging spectrometer 0.1-15keV
- Single Si chip array of 1024x1024 active pixels
- Pixel Pitch=100 μ m
- Area = 102x102mm² = 17.5'x17.5'
- 1 detector head (incl FW&FEE) & 2 HPP boxes on MIP
- 3 electronics boxes on FIP

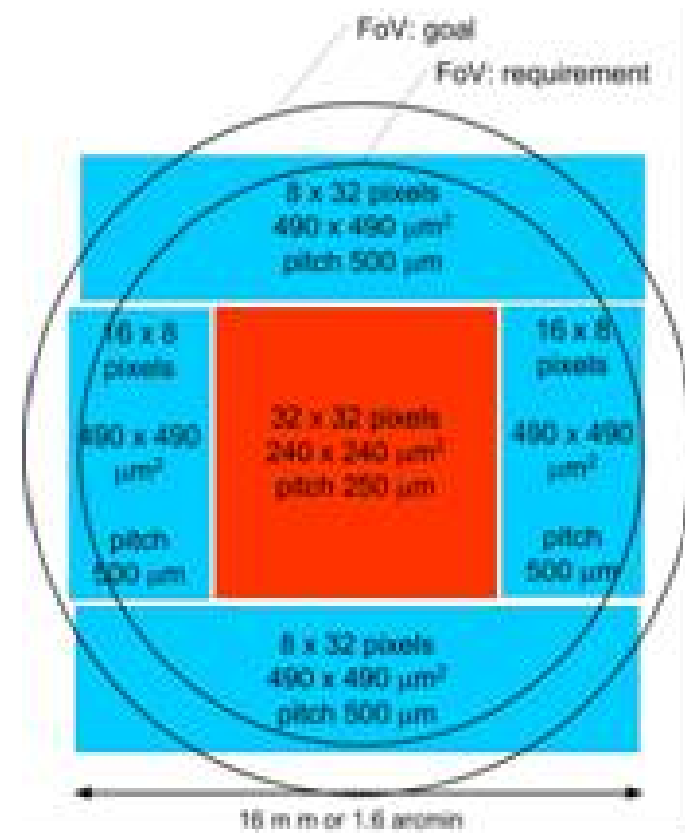
HXI specifications:

- 1 detector head & FEE + Analog electronics on MIP
- 2 Digital unit & PSU electronic boxes on FIP
- FOV = 12' circular



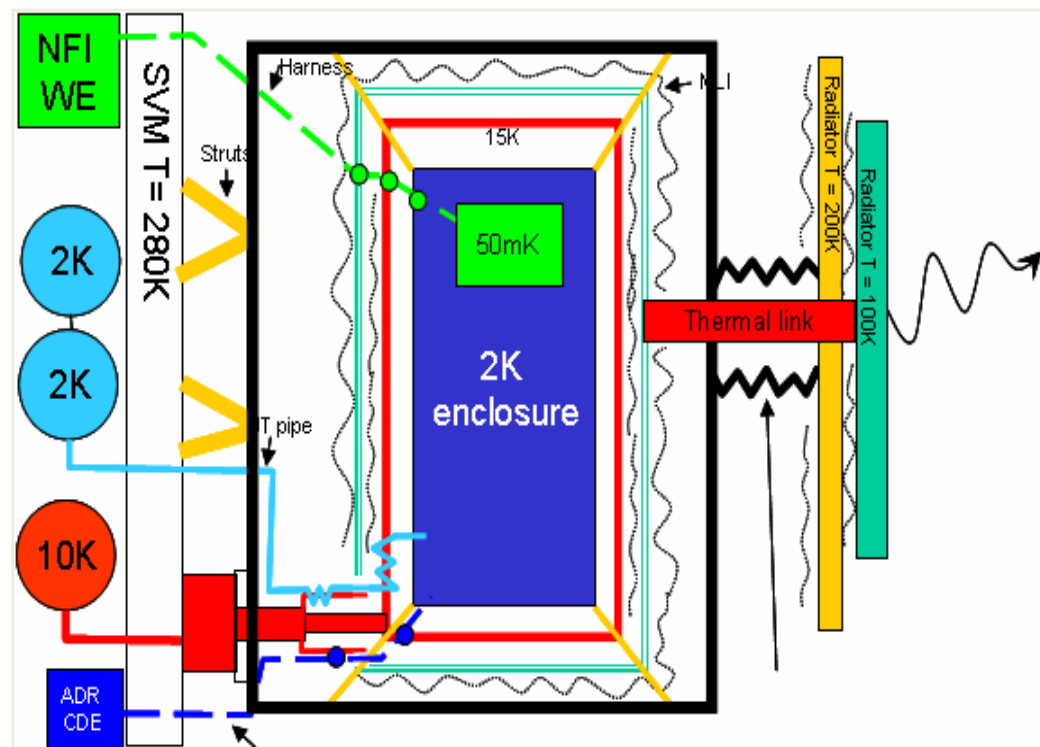
IXO instrument module: CIS

- Cryogenic imaging spectrometer based on TES
- Energy range = 0.1-10keV
- Inner array: 40x40 pixels ($300 \times 300 \mu\text{m}^2$), $\Delta E < 2.5 \text{ eV}$
- Outer array: 52x52 pixels ($600 \times 600 \mu\text{m}^2$), $\Delta E < 10 \text{ eV}$
- Total 2176 read-out channels
- $T_{\text{det}} = 100 \text{ mK} \pm 1 \mu\text{K}$ (50mK cooler I/F)
- FoV = $5.4 \times 5.4 \text{ arcmin}$
- CDF baseline: most demanding combination of European (NFI) and US (XMS) concepts
- Assumed US detector and Europe cooler
- Detector head + SQUIDs @ 50mK
- FEE + DE (RT) close to cryostat (on MIP)
- Event Processor, PSU, cooler controls @ RT on FIP



IX0 instrument module: CIS

- 280K cryostat + 100K radiator
 - 2 stage 10-15K Stirling cooler (2x)
 - 2-2.5K JT cooler (4x)
 - (300mK sorption cooler
+ 50mK ADR)
-
- Redundant pre-cooler concept
 - Relies on passive shield cooling
 - Cryostat @ RT -> simplifies I/F and testing



IXO instrument module: XGS

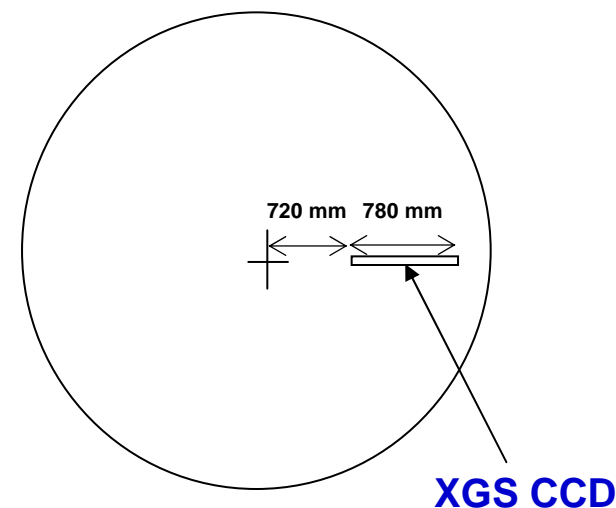
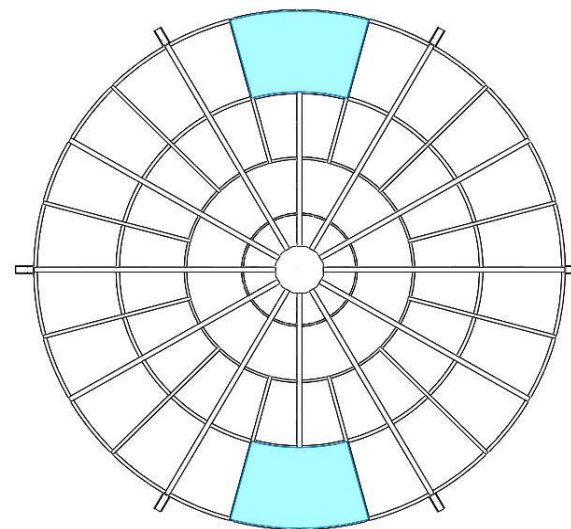
-> Instrument definition to be improved: PDD shall be updated with an XGS instrument description and interface requirement specification.

Grating box assumption:

- Selected $1.1\text{m} < R < 1.9\text{m}$ and two sectors of 22.5° each.
- Box dimensions $\sim 70 \times 80\text{cm}$ structure support Al $\sim 2\text{cm}$ deep (silicon grating only 3 microns thick)
- 2.4 kg incl 20% margin each box
- No attempt to address mounting to mirror, unit calibration, temperature constraints etc . . .

XGS camera assumptions:

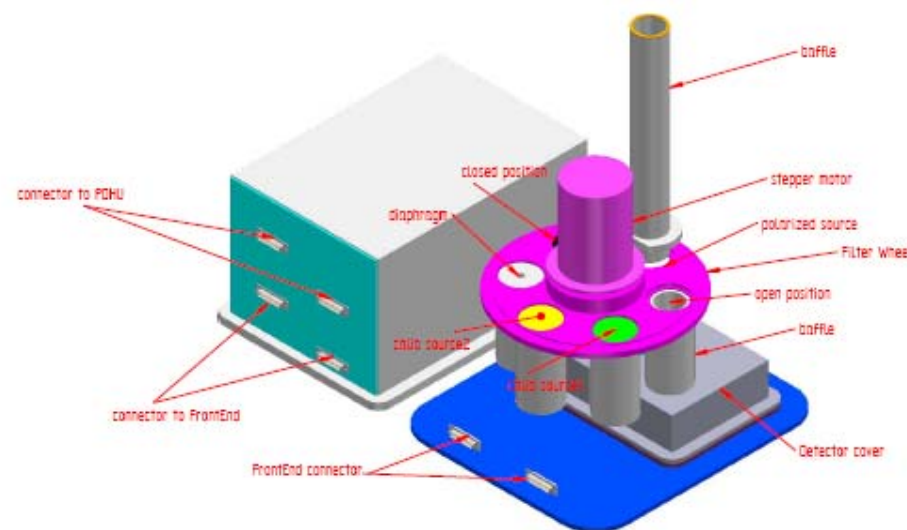
- Mass $\sim 20.4\text{kg}$ incl margins.
- Power $\sim 65\text{ W}$ incl margin + 3W CCD thermal control
- No translation stage needed at 3σ error level
- Refocussing mechanism needed



IXO instrument module: XPOL

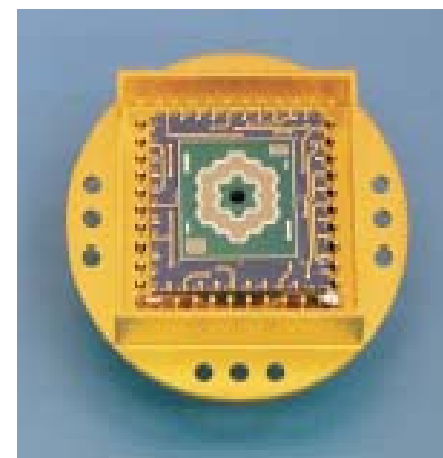
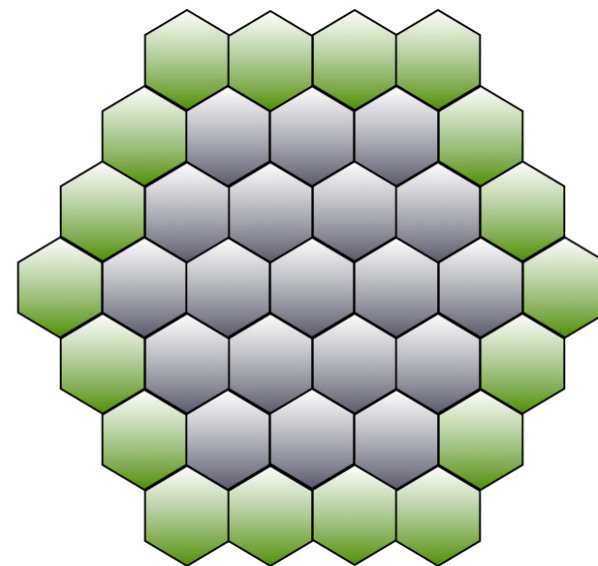
X-ray polarimeter based on scintillating gas cell

- Track detection gives polarization angle
- 300 x 352 pixels ($50 \times 43.3 \mu\text{m}^2$) = $15.24 \times 15 \text{mm}^2$
FOV = $2.6' \times 2.6'$
- $E=2\text{-}10\text{keV}$, $E/\Delta E=6$
- $T_{\text{det}}=283\text{K} \pm 2\text{K}$
- Room temp electronics
- 1 detector head + FEE & 1 back-end box all on MIP
- Harness: power & SpW



IXO instrument module: HTRS

- High time resolution spectrometer: $\sim 1\text{Mcps}$, $10\mu\text{s}$ resolution
- $0.5\text{-}20\text{keV}$
- based on 37 Silicon drift detector diodes – placed in defocused beam (182mm)
- $T_{\text{det}} = 253\text{K} \pm 1\text{K} [-40\text{C}, +35\text{C}]$
- 1 detector head + FEE & 1 electronic box on MIP
- Harness: power & SpW
- The instrument is non-imaging
- Multiple pixels are used for distributing the photons and achieving higher count-rate capability



IXO instrument module: resources summary

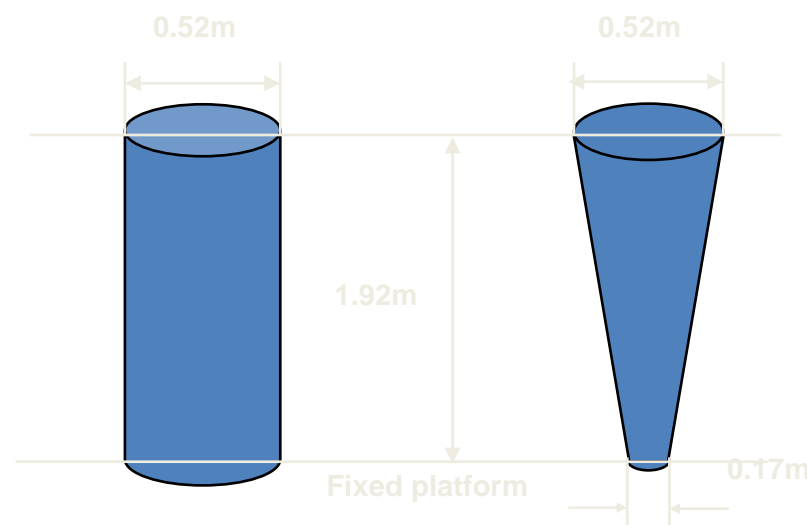
Instrument	Power	Mass	Data rate	Comment
WFI	280 W	90 kg	<1Mbps	
HXI	43 W	31 kg	<1Mbps	
XPOL	44 W	15 kg	<1Mbps	
HTRS	113 W	31 kg	MM	
NFI	521 W 576 W recycling	243 kg	<1.7Mbps	Incl cryogenics & 100K radiator
XGS	68 W	52 kg	158 kbps 1.8Mbps peak	Incl gratings & baffle
Total	993 W	462 kg		Power is worst case scenario

IXO instrument module: baffle

Stray light requirements:

- **visible/IR:**
 - XGS: $< 3 \times 10^8$ ph/s/cm² (200-1000nm)
 - CIS: $< 1 \times 10^8$ ph/s/cm² (TBC) (< 30 nm)
 - WFI: $< 1 \times 10^{12}$ ph/s/cm²
- **x-rays:**
 - Baffle should stop (to below particle background):
 - HXI/WFI/CIS: $E < 40$ keV (baffle+Au coating)
 - XGS: $E < 2$ keV (shroud is sufficient)

→ no direct view to sky other than through mirror



Mass (2mm CFRP, 200μm
LoS Au, 20% mounting)

- cylindrical : 20 kg
- conical: 12 kg

IXO instrument module: magnetic deflector

in instrument baffles (central baffle + XGS baffle)

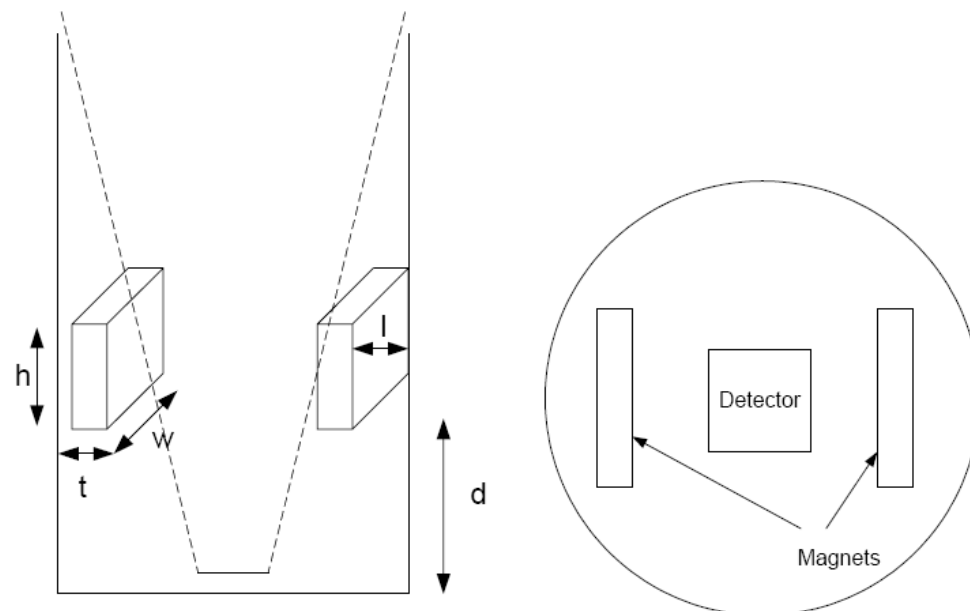
- Sized for deflection of all protons with in-band energy (after passing fixed filters) outside FOV:

WFI: $E_{\max} = 45 \text{ keV}$ FoV = 10 x 10 cm

CIS: $E_{\max} = 75 \text{ keV}$ FoV = 3.3 x 3.3 cm

XGS: $E_{\max} = 10 \text{ keV}$ FoV = 75 x 3 cm

- On-axis instruments:
 - magnets 10x15x2 cm,
 - Position 0.6m above detector
 - Residual field at detector ~5 Gauss!!
- XGS:
 - magnets 80x6x1 cm,
 - Position ~0.3m above detector



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IXO service module: power

- **Power subsytem:**
 - Max- power requirement: 4.5 kW
 - 28 V unregulated bus
 - 26.4 m2 deployable solar array (Ga As cells)
 - Li-ion battery (MA temperature control before Sun acquisition – 650 W during 2 h)
 - Power Distribution Unit (PDU) dedicated to instruments on the instrument platform

IXO service module: telecommunication

Telecommunication:

- 90 Gbs/day (including protocol over head)
- X bands around 8 GHz (10 MHz band)
- 8.7 Mbps with GMSK and RS (223,255)
- 3 h downlink/day
- Standard equipment: 10W RF power
 - 2 X/X transponder,
 - 2 TWTA,
 - 2 LGA,
 - 1 40cm HGA,
 - 1 RFDU
- New Norcia 35 m antenna G/S (baseline)
- Cebreros G/S (different hemisphere) used when needed, i.e. elevation too low or weather too bad in New Norcia)

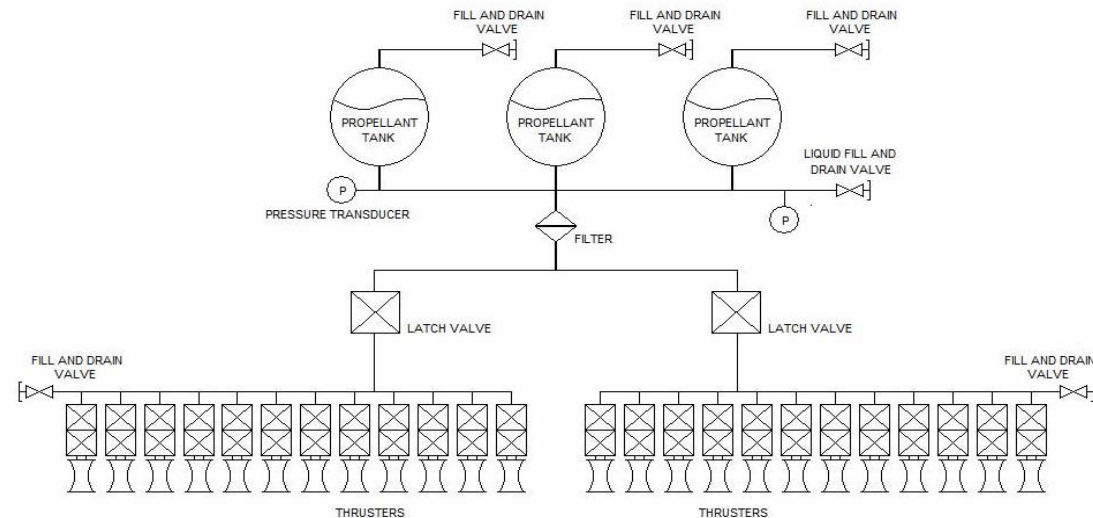
IXO service module: data handling

- **Data handling decentralized architecture:**
 - On Board Computer (OBC) located in the S/C Bus
 - Instrument Control Unit (ICU) located on the instrument platform for interfacing the IXO payloads/instruments
 - 2 x 250 Gbit memory using SDRAM technology located in the instrument platform
 - ICU interface the main S/C bus OBC by means of spacewire

IXO service module: propulsion

A Monopropellant system using Hydrazine (N_2H_4) is selected:

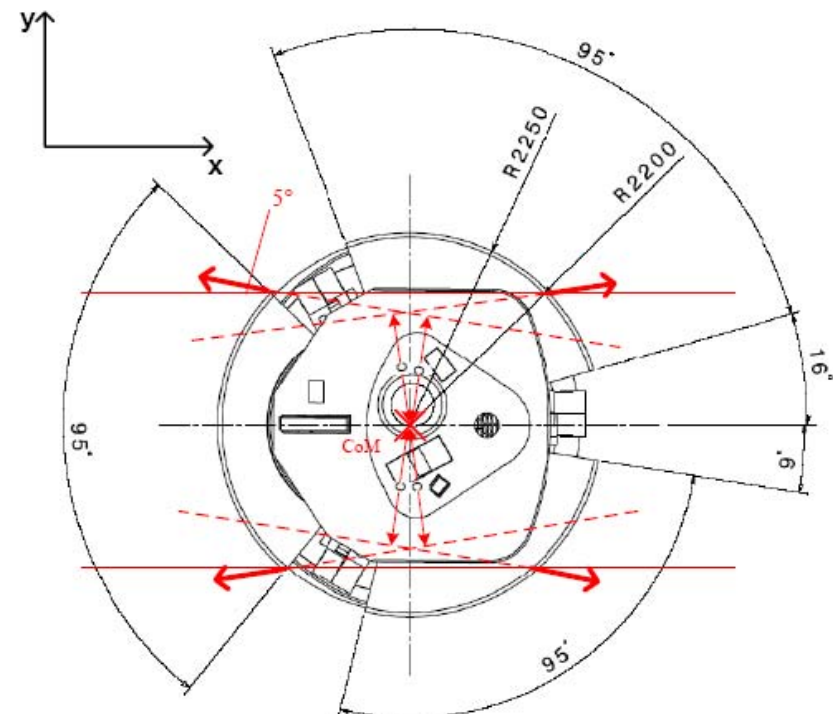
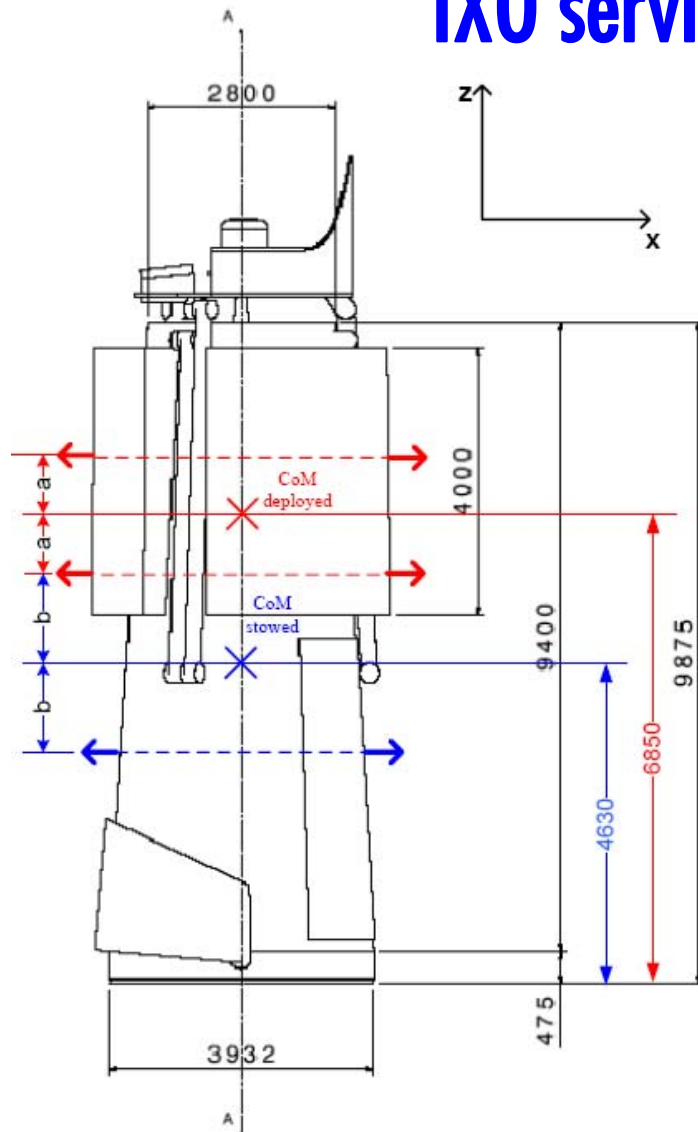
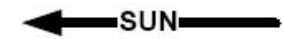
- 24 CHT-20 20N thrusters XMM – HP Astrium (D)
- 3 Titanium diaphragm tanks - Planck mission heritage (D)
- Sofrance filter (F)
- 2 Latch valve Moog (US)
- 2 Pressure transducers - Bradford(NL)
- 5 FDV/FVV Astrium (D)



If total Wet Mass = 6090 kg + total $\Delta V = 100$ m/s

then propulsion system = 59 kg dry mass + 334 kg propellant = 393 kg

IXO service module: propulsion



All thrusters are inclined by 5° in the x-y plane with respect to the x-axis.

Assumptions:

$a = 1000 \text{ mm}$
 $b = 1500 \text{ mm}$
 $c = 800 \text{ mm}$

2 x 12 thrusters with $F = 22 \text{ N}$ (incl. redundancy)

$\Delta V_x \rightarrow F_{\text{eff}} = F \times \cos(5^\circ)$

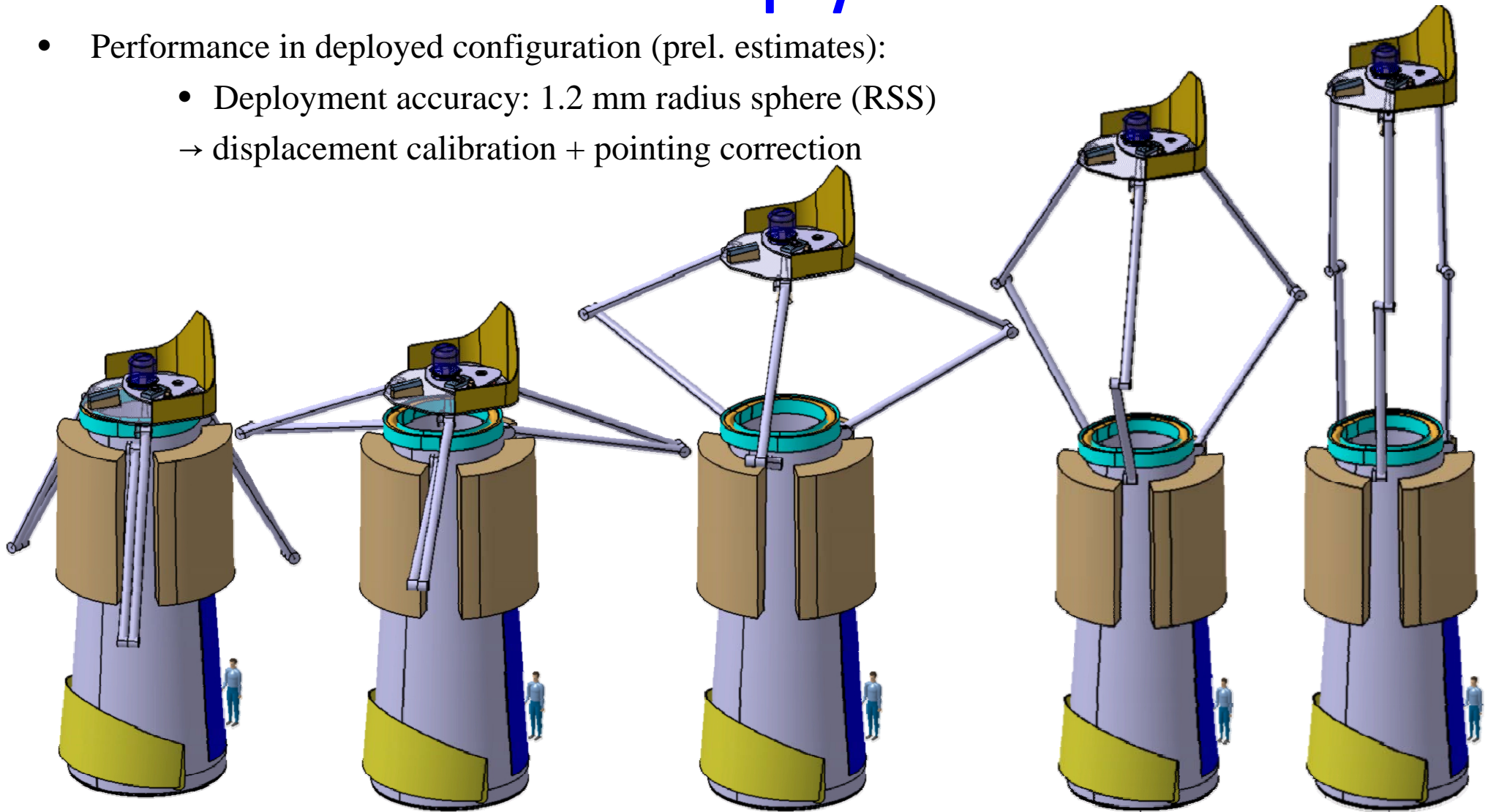
$\Delta V_y \rightarrow F_{\text{eff}} = F \times \sin(5^\circ)$

IXO service module: mechanisms

- Optical bench deployment mechanism (articulated boom concept)
- Instrument exchange and refocusing mechanism
- Mirror assembly deployable sun shield
- Inner mirror assembly retractable cover (TBC)
- Outer mirror assembly ejectable cover
- High gain antenna pointing mechanism
- Solar array deployment mechanism

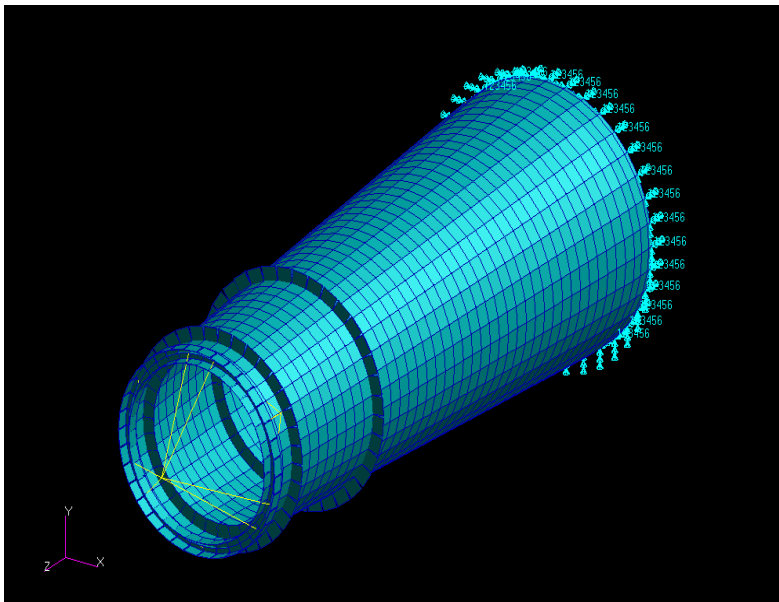
IXO service module: deployment mechanisms

- Performance in deployed configuration (prel. estimates):
 - Deployment accuracy: 1.2 mm radius sphere (RSS)
→ displacement calibration + pointing correction

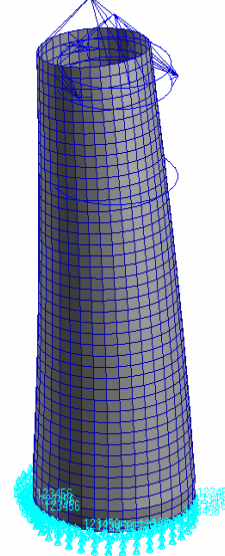


IXO service module: deployment mechanisms

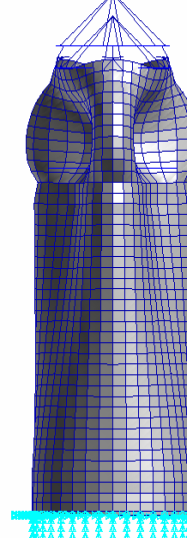
	Eigen Frequency (Hz)			
	Requirement			
Direction	Ariane 5	Atlas 5	FEM Target	FEM Result
Lateral	8.50	TBD	9.78	9.72
Longitudinal	27.00	TBD	31.05	44.47



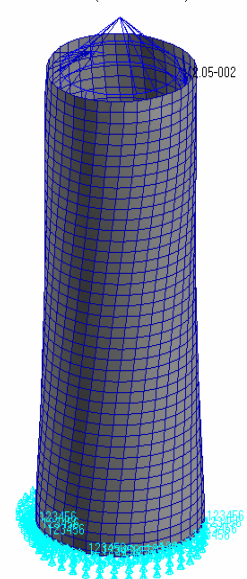
arvectors, Translational, (NON-LAYERED)



ctors, Translational, (NON-LAYERED)



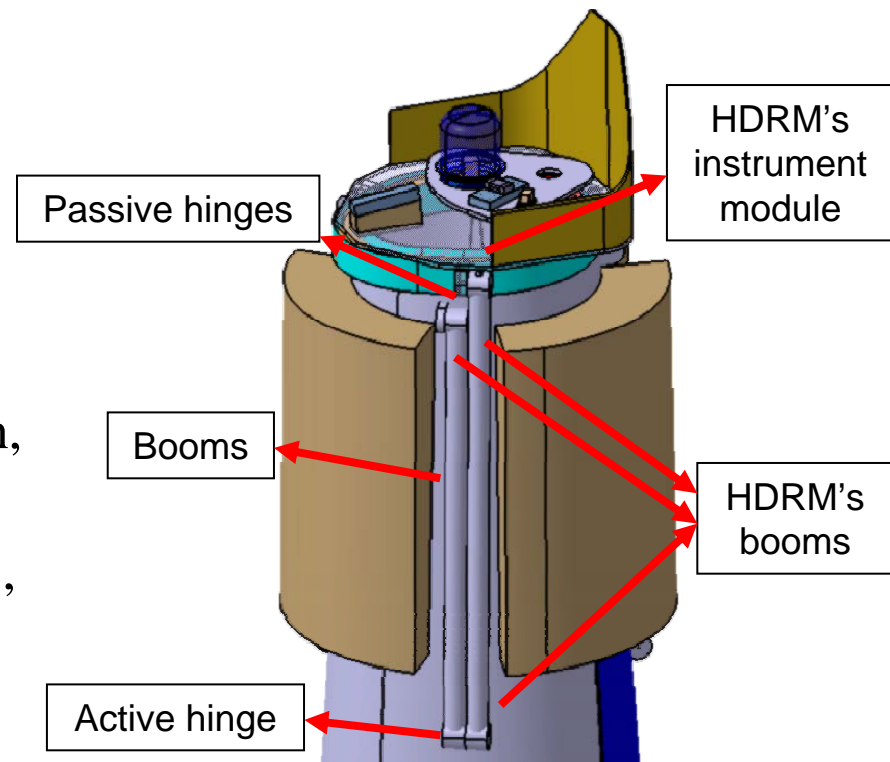
vectors, Translational, (NON-LAYERED)



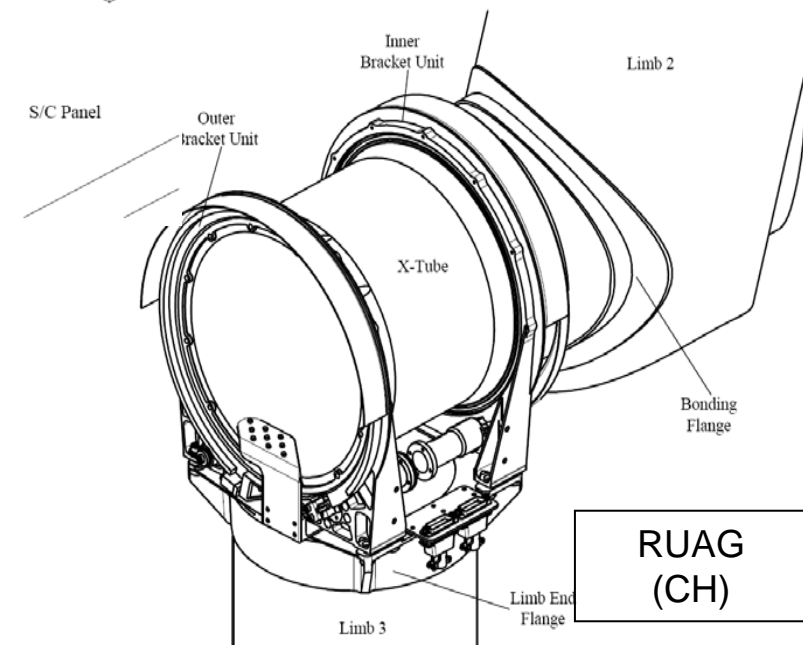
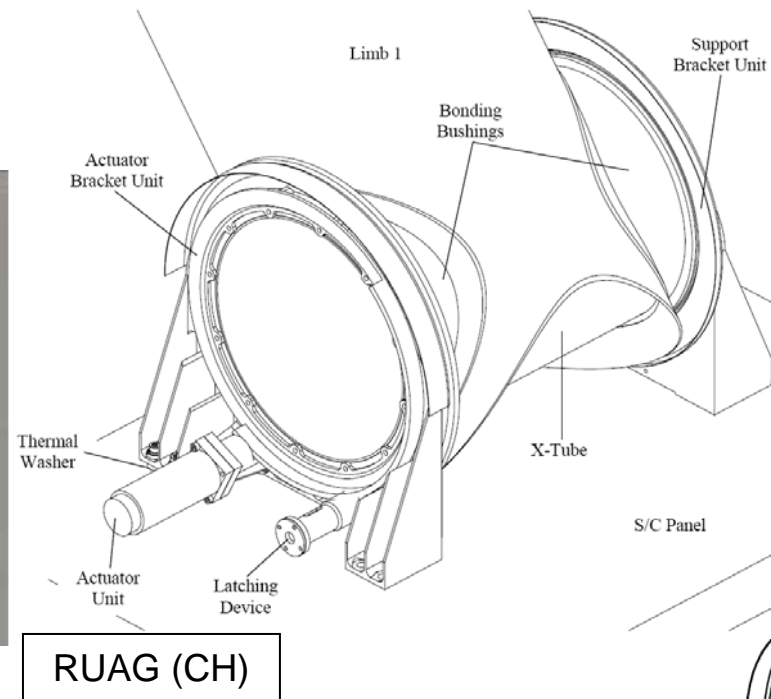
IXO service module: deployment mechanisms

Areas of concern for OB deployment mechanism:

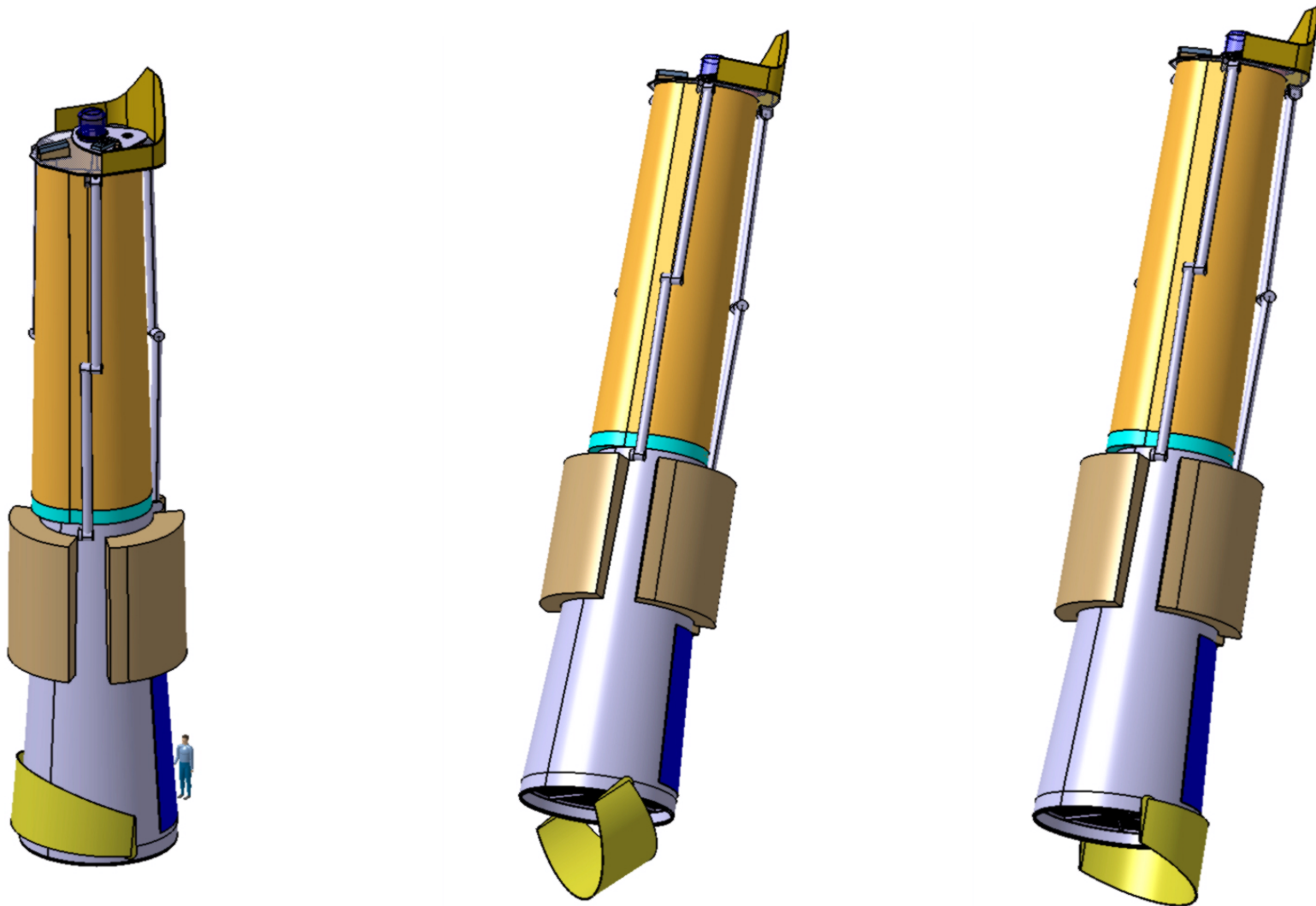
- Stowed configuration:
 - Number / location of hold-down and release mechanisms
- During deployment phase:
 - Adequacy of actuation torque
 - Misalignment / lack of synchronization between arm, thus high stresses, friction, potential jamming, due to :
 - initial alignment errors (on ground),
 - errors during actuation,
 - thermo-elastically induced distortions,
 - dynamic perturbation



IXO service module: deployment mechanisms



IXO configuration



Shroud Scale Model

- The GSFC Blanket shop created this 1/25th scale prototype.
- Stows to 3.5cm with some compression force.
- Extends to 49cm nominally.
 - Can extend to about 65 cm with force, but risks tearing the corner seams.
- Stows to about 7% of nominal extension length.
(3.5/49)

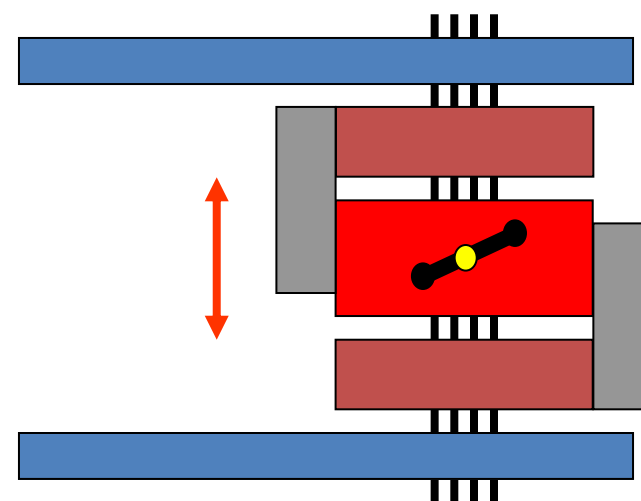


49 cm
65 cm max

14.5 cm ID
18 cm OD

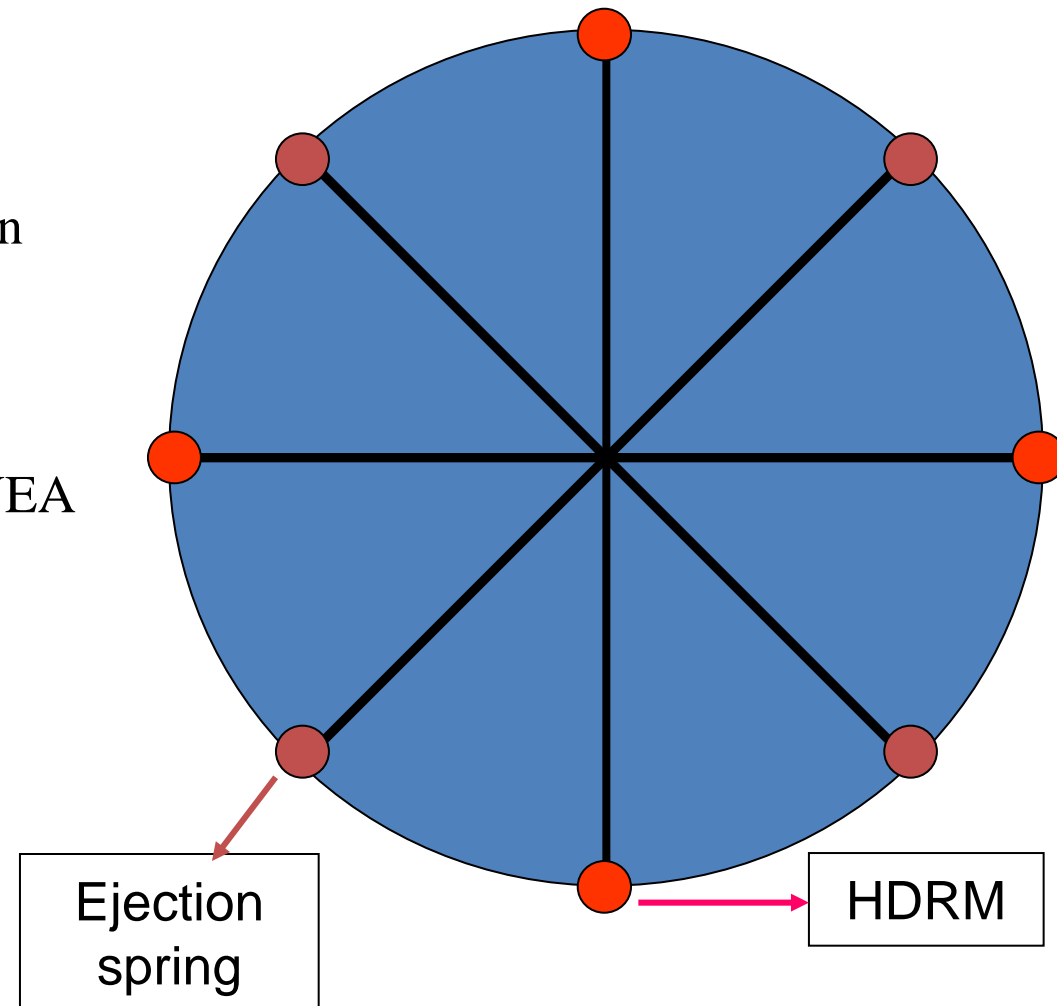
Instrument exchange and refocusing mechanism

- Integrated mechanism for rotational and linear movement
 - Two rotational drives
 - Stepper motors with angular encoders
 - Torque of 90 Nm (TBC-Harness definition missing)
 - Accuracy of 0.01 deg
 - Tilted slots and rolling elements for refocusing
 - Stroke of ± 5 mm
 - Accuracy of 0.1 mm
 - Harness routing for minimal torque
 - Temperature controlled
 - $> -20^{\circ}\text{C}$ operational temperature
 - Life: approx 2000 cycles



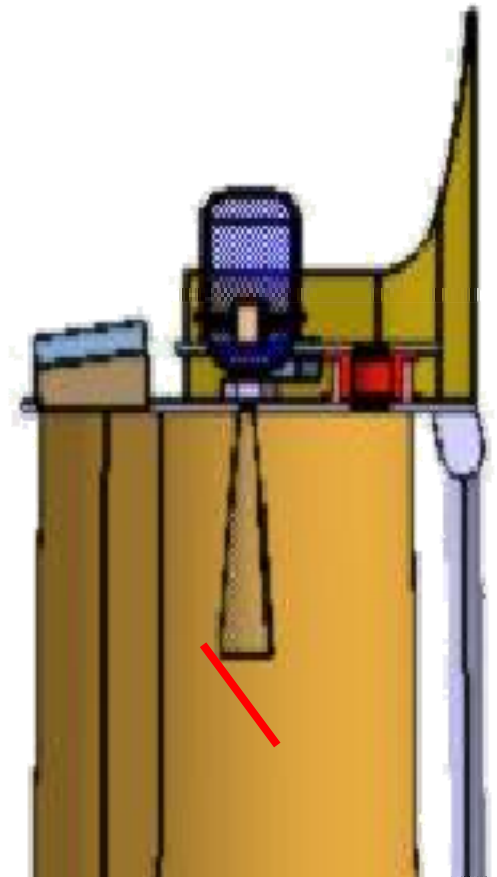
Mirror contamination protection

- Outer mirror assembly protection
 - Outer mirror assembly cover ejection mechanism
 - 4 springs
 - Ejection velocity 0.3-0.5 m/s
 - 4 x Non-explosive separation nut (NEA electronics)
 - Internally redundant
 - Quasi-simultaneous release



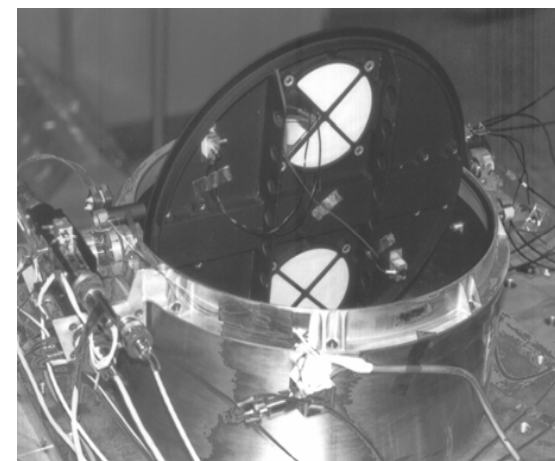
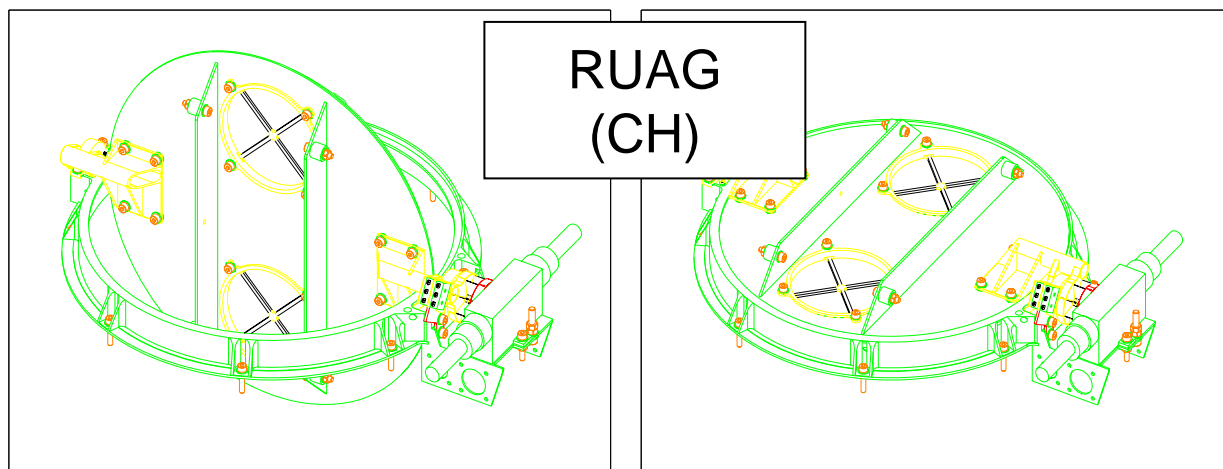
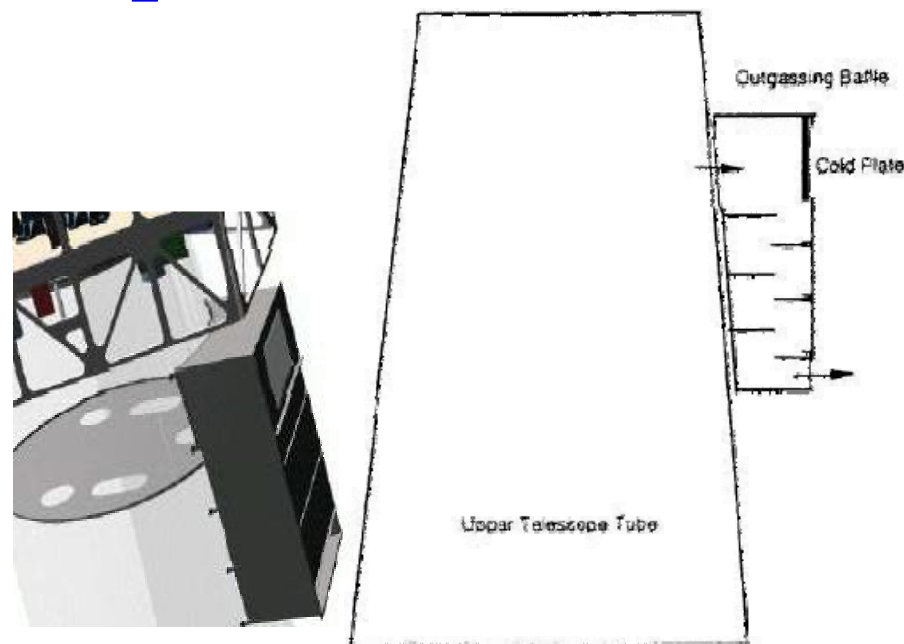
Mirror contamination protection

- Inner mirror assembly protection (Baseline)
 - Cover mirror during assembly
 - Eliminate sources of contamination
 - Main source: Electronic boxes on the inside of the instrument module
 - Overpressure telescope inner volume (N_2)
 - Mechanism to close focal point hole on the baffle inside
 - HDRM: Thermal knife
 - Deployment spring



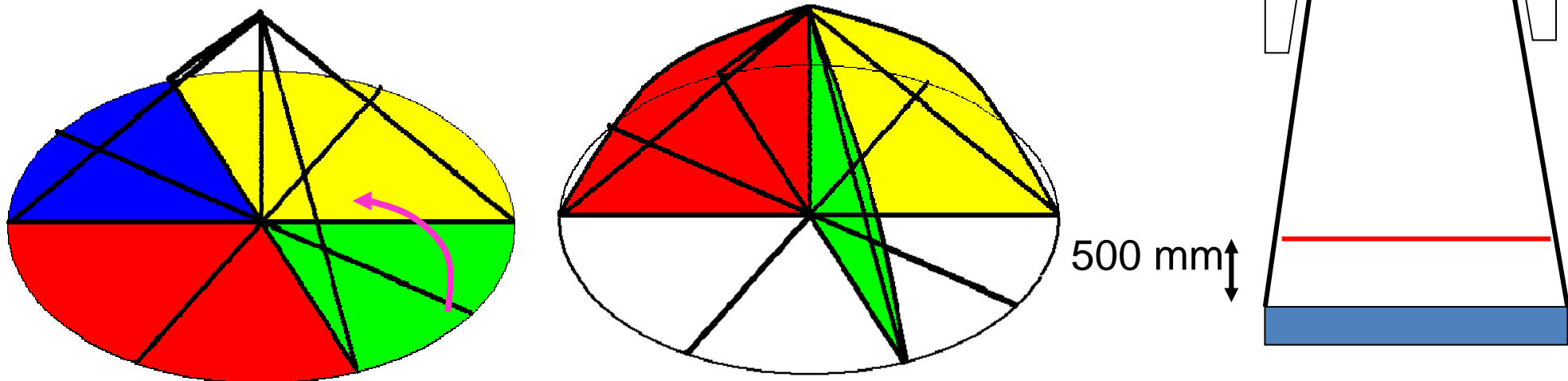
Mirror contamination protection

- Inner mirror assembly protection (Baseline)
 - Venting mechanism
 - Two venting and outgassing doors (XMM Newton)
 - Outgassing baffle (XMM Newton)



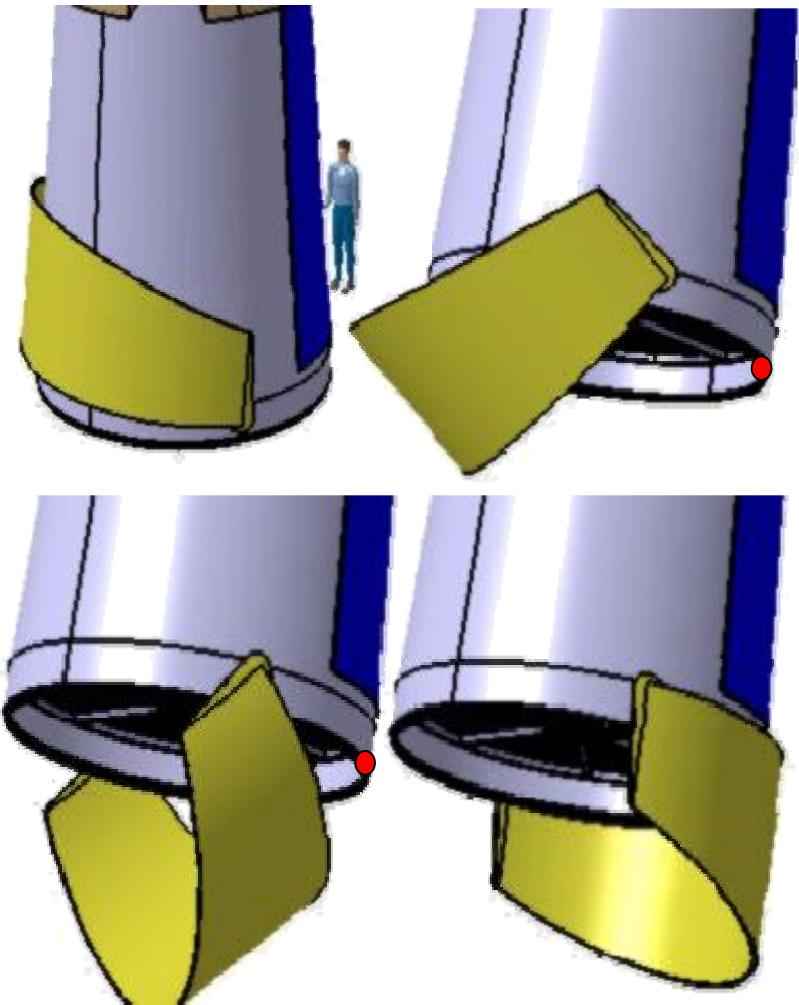
Mirror contamination protection

- Inner mirror assembly protection (Option / addition)
 - Deployment springs
 - 4 x 3 Thermal knives (Dutch space)
 - Dampers
 - Seal ring
 - Feasibility? Interface with XGS?



Mirror assembly sunshield

- Rotating mirror baffle (Baseline)
 - Two deployment springs
 - 4 x Thermal knives (Dutch Space)
 - Locking mechanism at the center of baffle half circle
- Inflatable structure (Option)



IXO service module: attitude and orbit control system

- **GNC Architecture : 3 modes**
 - Acquisition and Safe Hold (ASH) mode
 - Acquire Sun on +X axis
 - Fine Pointing and Slew (FPS) mode
 - Hold inertial pointing towards target
 - Target change manoeuvre
 - Note: use also during cruise
 - Thruster Control Maneuver (TCM) mode
 - Trajectory correction, orbit maintenance and wheel off-loading

IXO service module: attitude and orbit control system

- **GNC Equipments**

- Actuators

- Honeywell reaction wheel: HR16 (120 Nms) @ 0.2 Nm Note: possible alternative Goodrich TW-125E200
 - 5 reaction wheel (including 1 on Y-axis)
 - EADS monopropellant thruster: 22 N

- Sensors

- Sodern autonomous star tracker: Hydra
 - TNO fine sun sensor (calibrated bias error: 0.01°)
 - TNO sun acquisition sensor (accuracy $< 1^\circ$)
 - SAE MEMS rate sensor (rate bias drift $< 5^\circ/\text{hr}$)
 - Alignment Monitoring Camera (AMC): Sodern coarse lateral sensor (derived from Hydra star tracker) FoV: 1° – accuracy $< 1''$



IXO service module: attitude and orbit control system

42° (No. of slews / year: 250)	[day]	40.0	Settling time allocation: 5 min
180° (No. of slews / year: 10)	[day]	5.4	Settling time allocation: 5 min
Momentum management (every 2 days)	[day]	0.05	Settling time allocation: 2 min
L2 orbit maintenance (every month @ 4 hr)	[day]	2.05	Settling time allocation: 3 min
Detector (No. 41 @ 60 s)	[day]	0.03	Settling time allocation: 1 min
TOTAL	[day]	48.3	
Science	[day]	316.7	
Operational Efficiency	%	86.8	

IXO service module: attitude and orbit control system

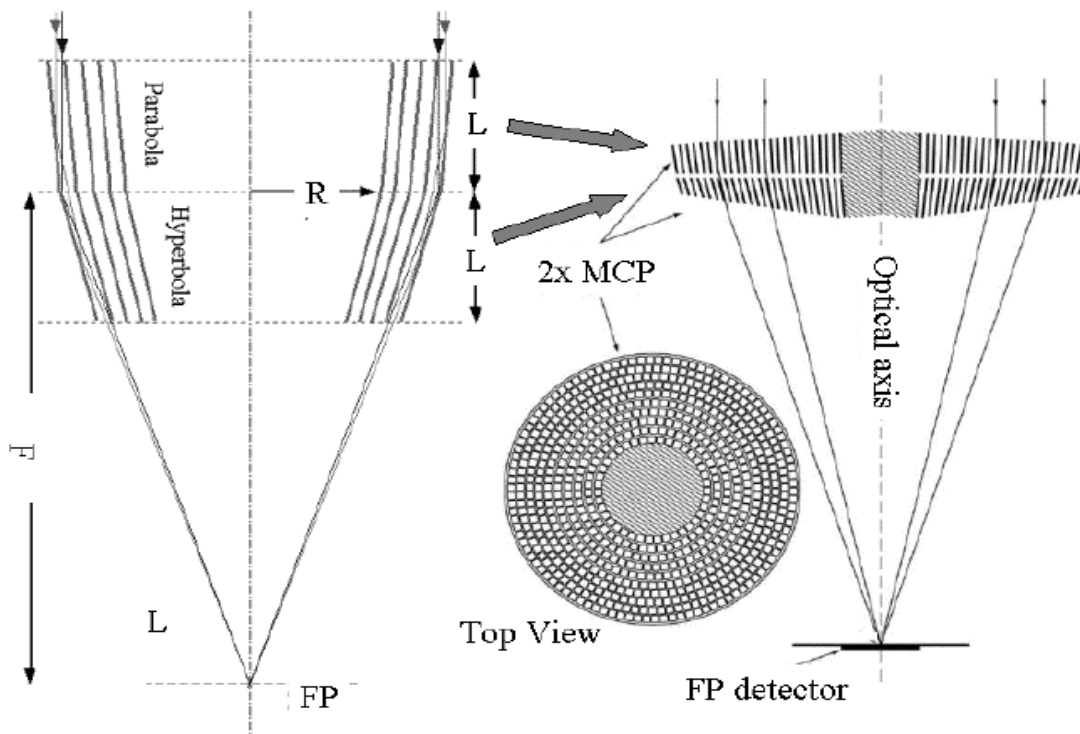
- Onboard pointing requirements (after stabilization)
 - (LT, MT) STR vs MA alignment 1.0 arcsec
 - (LT, MT, ST) STR measurement errors **4.0 arcsec**
- Preliminary image quality budget
 - (MT) STR vs MA alignment 0.3 arcsec¹
 - (MT) STR measurement stability **1.0 arcsec**
- Preliminary astrometry budget
 - (MT) STR vs MA alignment 0.3 arcsec¹
 - (S, LT) STR vs MA alignment 0.3 arcsec¹
 - (S, ST) STR residual bias **0.5 arcsec**
 - (S, ST) Residual STR measurement noise **0.1 arcsec**

¹ similar requirements for the Alignment Monitoring Camera

IXO mission concept

- 1 – Introduction
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- 7 – IXO mirror assembly**
- 8 – Options
- 9 – Conclusion

IXO mirror assembly: specification requirements



Pore optics technology

Double-conical approx to Wolter I

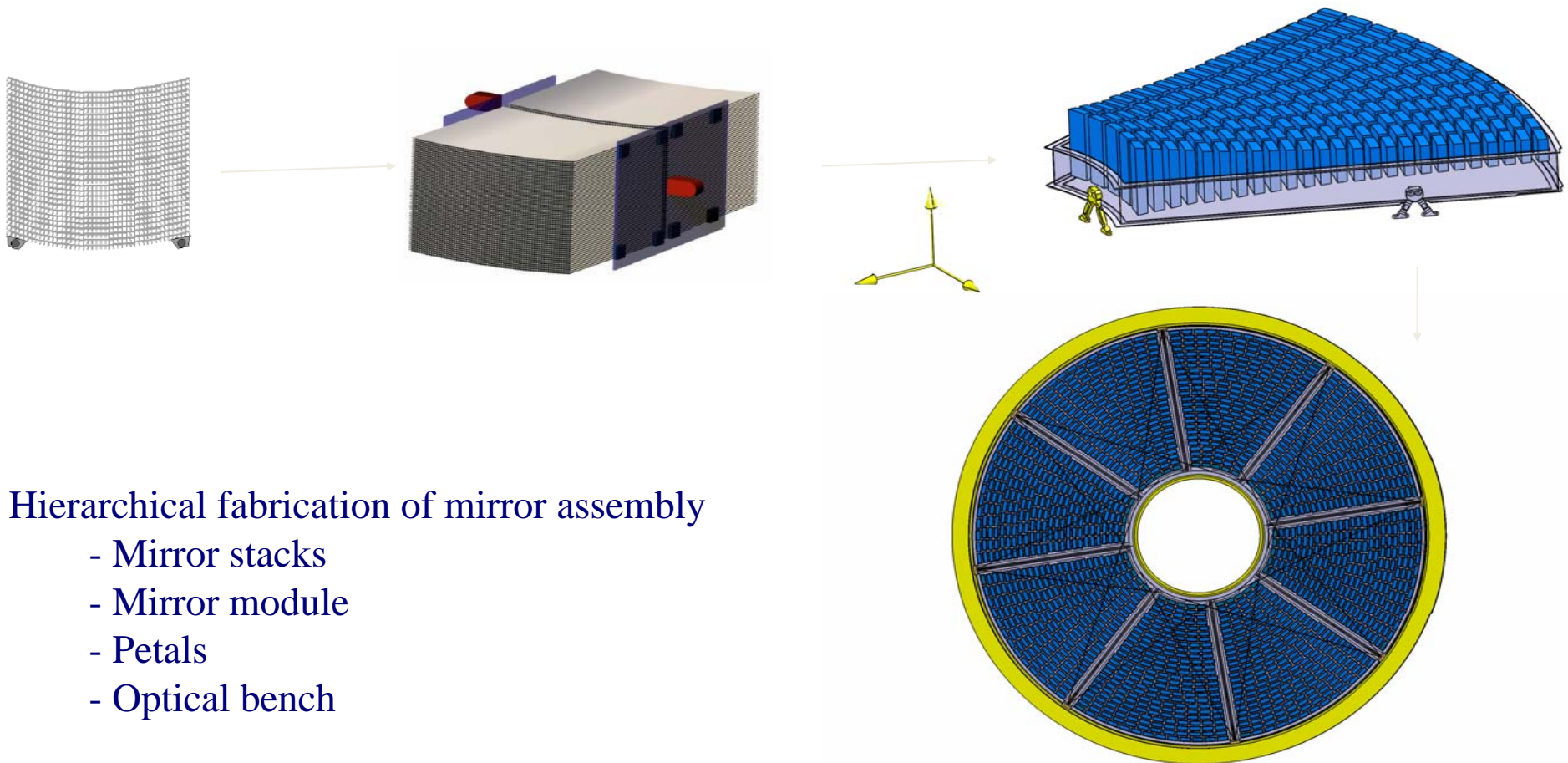
$F = 20 \text{ m}$

$\text{FOV} = 17.5 \times 17.5 \text{ arcmin}$

Coating:

- Iridium + C overcoating (outer shells)
- Multilayer coating (inner shells ($\theta < 0.27^\circ$))

IXO mirror assembly: manufacturing concept

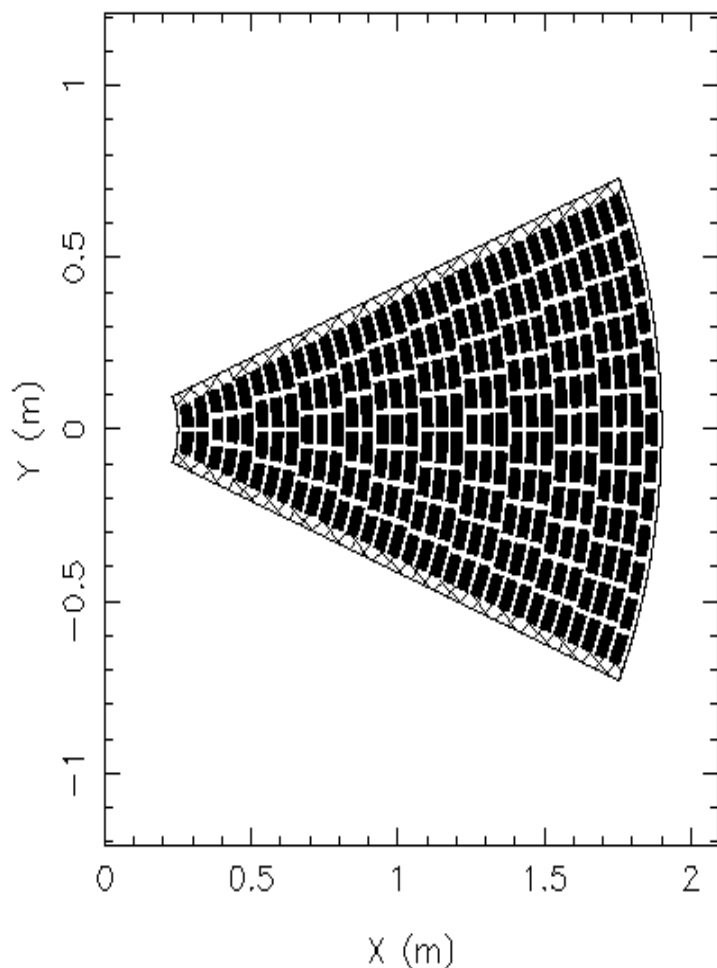


Hierarchical fabrication of mirror assembly

- Mirror stacks
- Mirror module
- Petals
- Optical bench

IXO mirror assembly: optical design

F: 20.0m Rin: 0.25m Rout: 1.90m Nr. of Petals:



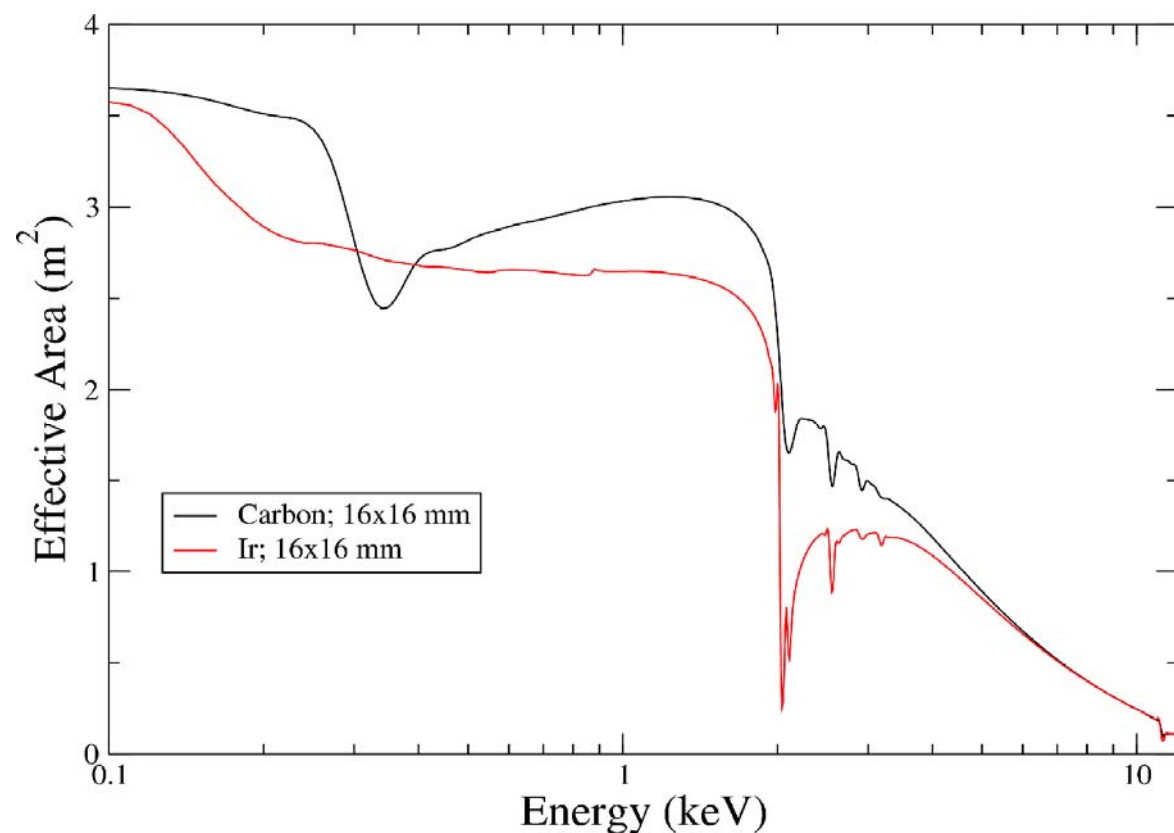
Optical design assumption:

- Inner radius 0.25 m, outer radius 1.90 m
- 32 rows
- 236 mirror modules/petal
- spoke width (7cm)

→ **To achieve the 3m² A_{eff} requirements, the azimuthal/radial spacing of the mirror modules shall be ≤16 mm** (22mm assumed for XEUS)

--> The compatibility of the optical bench structure with the allocated mirror module spacing, mass, spoke width and launch loads has to be demonstrated by FEM analysis.

IXO mirror assembly: performance estimate (TBC)



Without C overcoating:

Aeff (1.25 keV) ~ 2.6 m²

Aeff (6.00 keV) ~ 0.65 m²

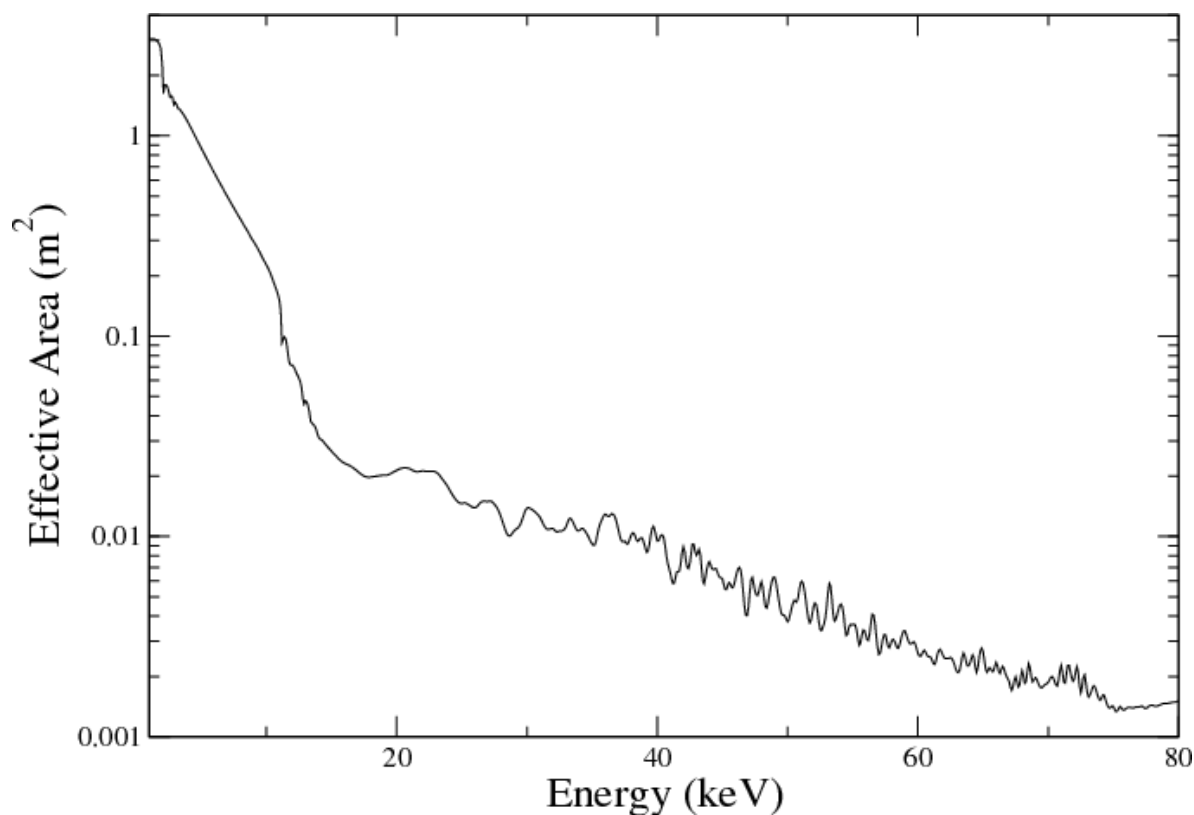
With 90 Angstrom C overcoating:

Aeff (1.25 keV) ~ 3.0 m²

Aeff (6.00 keV) ~ 0.65 m²

To achieve the 3m² Aeff at 1.25 keV requirements, the mirror modules shall be covered with a C overcoating

IXO mirror assembly: performance estimate (TBC)



**With JAXA/ISAS multilayer design
(courtesy H. Kunieda):**

$A_{\text{eff}}(30 \text{ keV}) \sim 150 \text{ cm}^2$

Mirror Module Thermal Control

- About 2[kW] heater power needed to operate the mirror assembly at high temperature (feasibility of room temperature operation is TBC for pore optics)
- A pre-collimator is foreseen to control the radiative environment in front of each individual mirror module
- A post collimator is foreseen to control the temperature gradient that will be induced by the inner conical structure.
 - Interface with grating spectrometer? thermal control of grating spectrometer?
- The Sunshield is covered with MLI on external side and SSM on internal side (TBC) for a mass estimated at 10[kg].
- The current thermal control system and configuration allows a slow rate of temperature drop (7.5[K]/hr)

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IXO mission concept: increased focal length

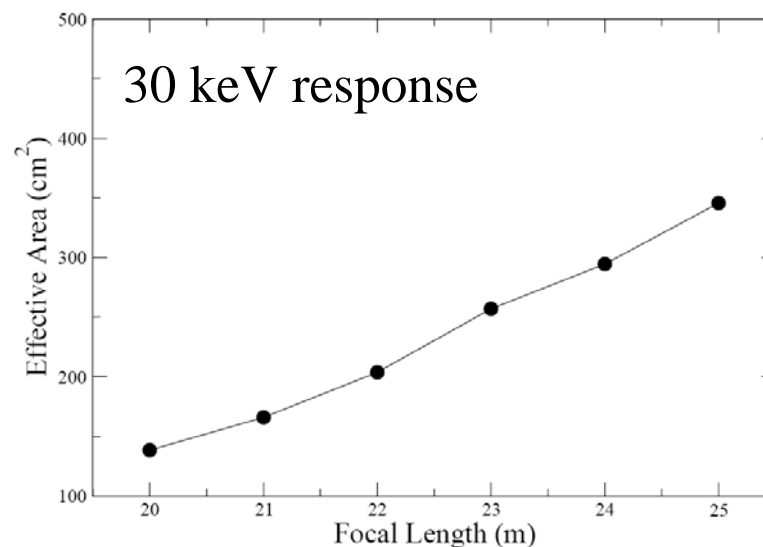
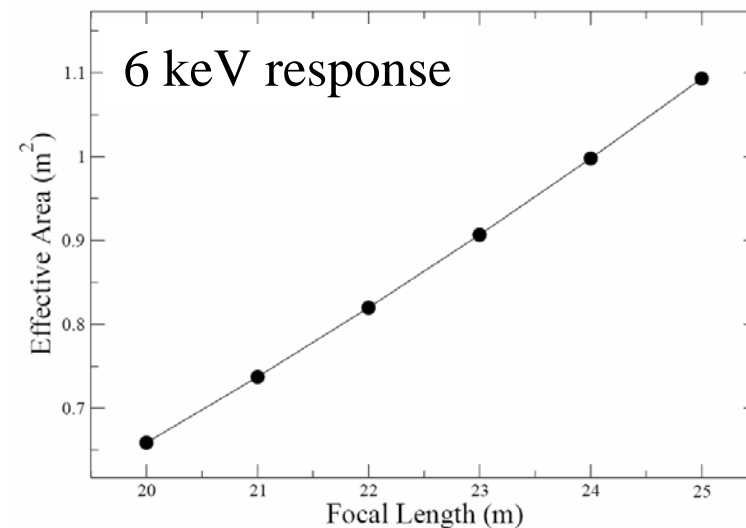
Increased focal length → mass increase

→ Mass to be taken on:

- mirror assembly:
- instruments:

CSI
or XGS without shroud

→ Large impact on the system



IXO mission concept: retractable grating box

Mirror assembly and CAT grating accommodation still to be studied:

- Mirror assembly optical design (**pore optics**) concept
- Mirror assembly petals and optical bench mechanical concept
- Mirror assembly thermal control (e.g. pre and post collimator, heaters)
- Mirror assembly contamination control (e.g. telescope cover, inner cover if needed)
- Grating box concept and interface requirements (NASA input to PDD)
- Definition of mirror assembly interface with grating spectrometer
- Grating accommodation concept
- Prospective achievable X-ray performance

Retractable grating concept option still to be studied:

- Difficulties anticipated: mechanism concept and reliability, XGS thermal control, accommodation/ interface with post collimator outer cover if needed

→ No solution identified during the CDF

IXO mission concept: X-ray events time stamping accuracy

- The GAIA installations for the pure timing accuracy can be reused:
1.2 μs timing accuracy (excluding orbital accuracy induced errors)
- Orbital accuracy induced errors:

pass duration* [h]	$\delta\rho$ [km] (1 σ)	$\delta \mathbf{r} $ [km] (1 σ)	δt_p [μs] (1 σ)	δt_r [μs] (1 σ)	δv_p [mms $^{-1}$] (1 σ)	δv_r [mms $^{-1}$] (1 σ)
8	0.02	0.5	0.07	1.7	0.5	1.5
4	0.02	0.5	0.07	1.7	0.7	1.5
2	0.02	0.7	0.07	2.3	0.9	2.0
0.5	0.02	2.0	0.07	6.7	1.0	2.5

*plus 0.5h ranging

IXO mission concept: X-ray events time stamping accuracy

- 0.5 h pass (0.5h Doppler and 0.5h ranging):

$$\delta t_{t+p+|r|} = \text{SQRT}(1.2^2 + 0.07^2 + 6.7^2) = 7 \mu\text{s}$$

- 2 h pass (2h Doppler and 0.5h ranging):

$$\delta t_{t+p+|r|} = \text{SQRT}(1.2^2 + 0.07^2 + 2.3^2) = 2.5 \mu\text{s}$$

⇒ 10 μs 1 σ achievable even with very short daily passes

⇒ 2h passes allow for higher accuracy (or for coverage gap of up to 2 days)

Time and position reconstitution requires post processing of measurements by Flight Dynamics, i.e. precision data are only available a posteriori (~ week after the fact)

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IXO mission concept: conclusion

An IXO mission concept has been established that is:

- technically promising (no show-stopper identified)
- modular and well-suited to an International collaboration

The deployable IXO mission concept presents some risks:

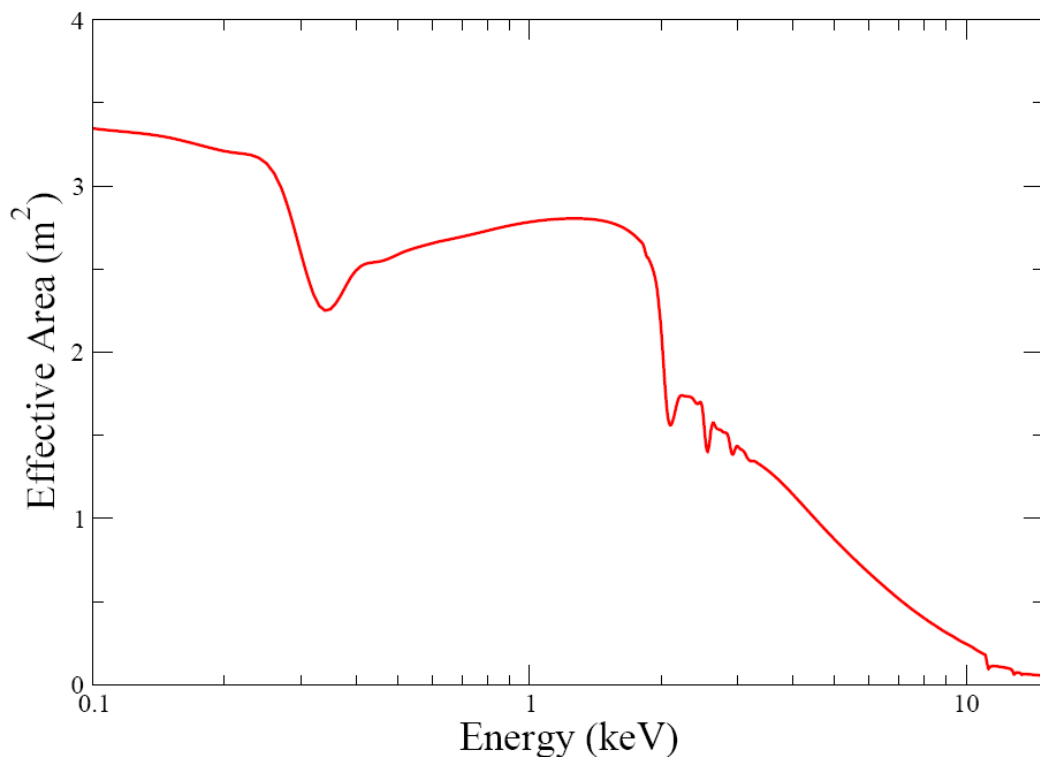
- large number of experiments
- large number of deployable mechanisms
- complex collaboration set-up (high cost risk)

Highest technical risk areas include:

- mirror technology and overall mirror assembly (including grating accommodation),
- CSI (including cryogenic chain),
- bench deployment mechanism,
- instrument exchange mechanism,
- shroud (deployment and micrometeorites impact/straylight)
- mirror assembly cover/ front sunshield deployment
- instrument alignment vs mirror assembly/ metrology

IXO mission concept: conclusion

IXO CDF mission concept prospective performance (feasibility to be assessed):



IXO A _{eff}	Science Objectives	Estimated Performance
1.25 keV	3 m ²	2.8 m ²
6 keV	1 m ²	0.65 m ²
30 keV	350 cm ²	150 cm ²

Assuming:

- Fixed grating assembly with A_{eff}= 1000 cm²
- MA mass compatible with 1735 kg allocation
- 16 mm MM spacing compatible with launch load
- Carbon overcoating on mirrors
- 50 ppm dust and 1 Å microroughness (optimistic)

--> feasibility to be assessed

IXO mission concept: conclusion

IXO open issues:

- Mirror assembly opto-thermo-mechanical design/ performance
- XGS instrument definition and interface requirements (input to PDD)
- XGS grating box accommodation
- Optical bench deployable mechanism → performance/risks/ reliability
- Deployable shroud / micrometeorites impact → stray-light
- Grating box retractable mechanism/ effective area at low X-ray energy

→Post CDF activities:

- Mirror assembly opto-thermo-mechanical design/ performance
- AOCS performance estimate (effect of deployed bench and solar array)
- Deployable mechanism dynamic analysis
- Straylight analysis (TBC)
- L2 particle environment